

# Corso di Misure a Microonde

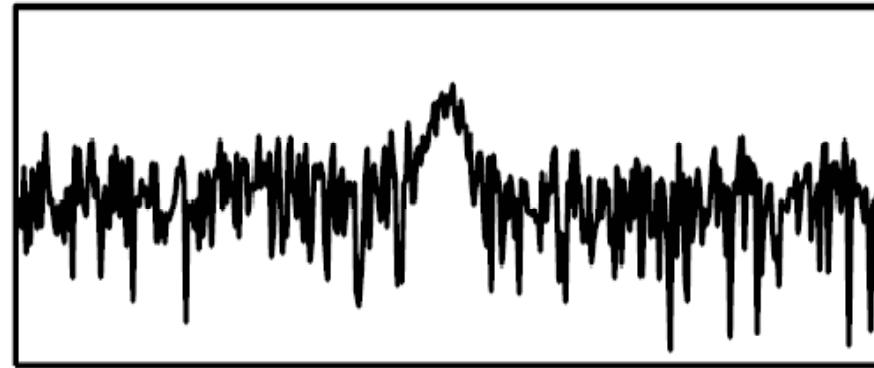
## Misure di potenza

Prof. Luca Perregini

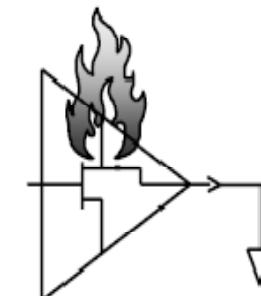
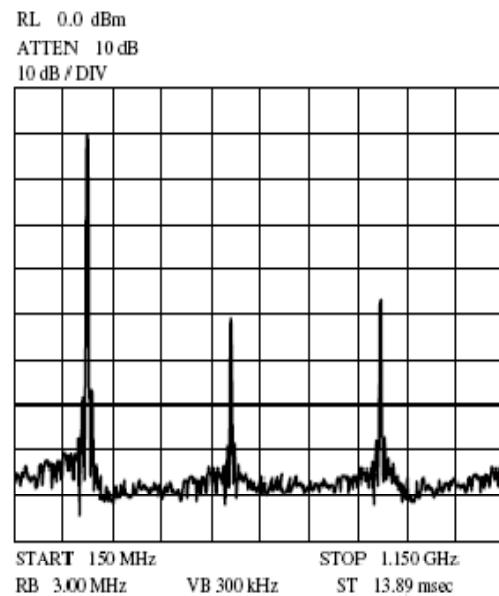
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# Importance of Proper Signal Levels

- Too low
  - Signal buried in noise



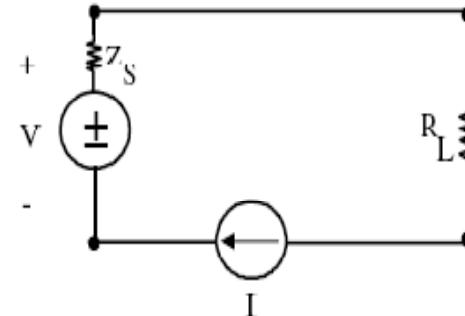
- Too high
  - Nonlinear distortion can occur



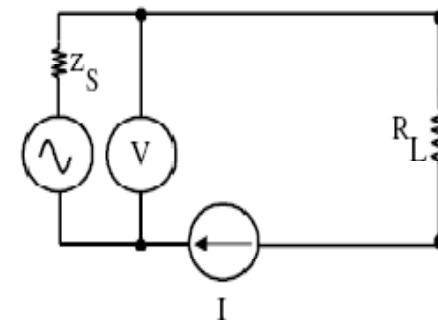
- Or even worse!

# Why Not Measure Voltage?

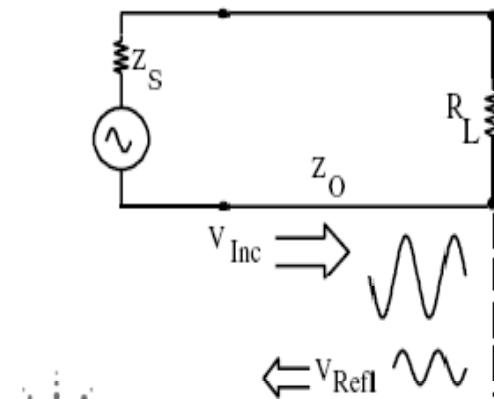
- DC



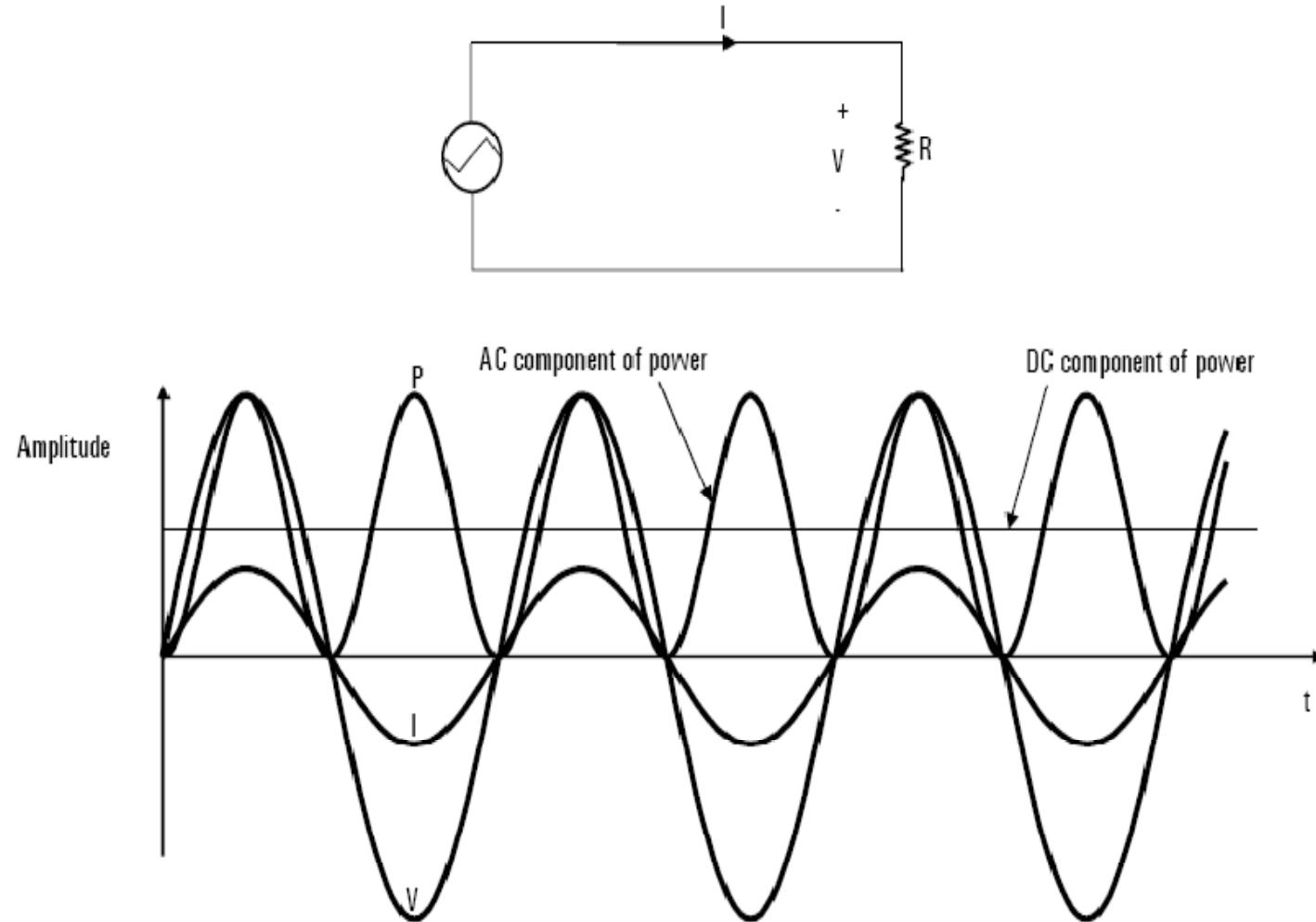
- Low Frequency



- High Frequency

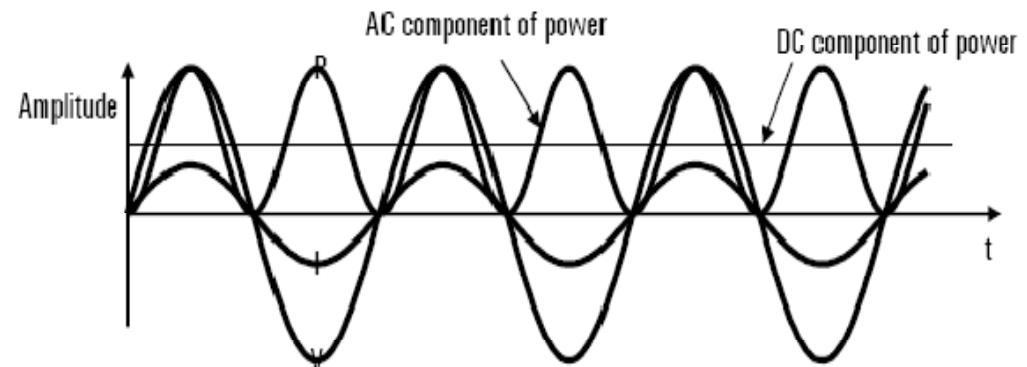


# Power: $P = V I$



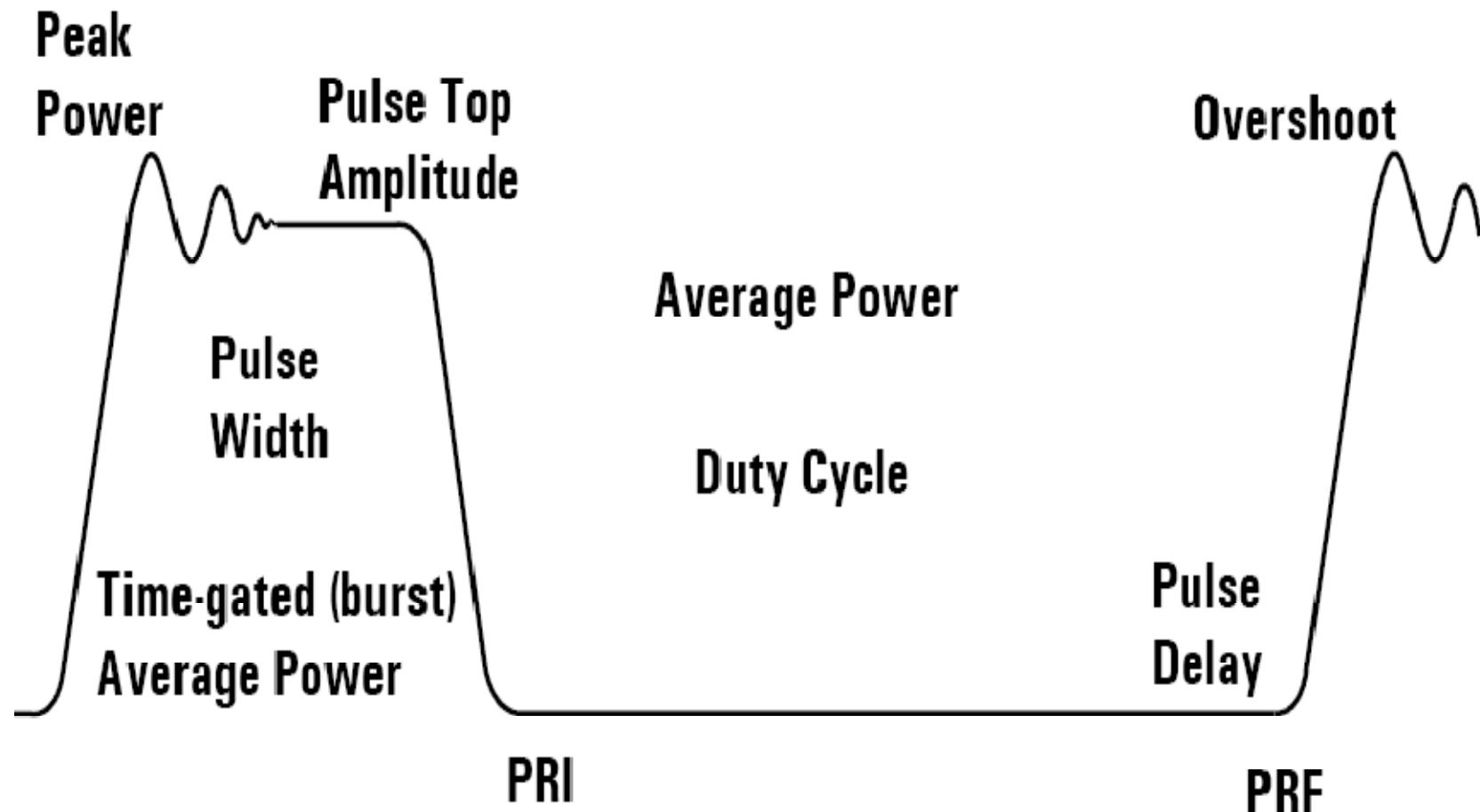
# Units and Definitions

Power:  $P = (I)(V)$



- Unit of power is the watt (W):  $1W = 1 \text{ joule/sec}$
- Some electrical units are derived from the watt:  
 $1 \text{ volt} = 1 \text{ watt/ampere}$
- Relative power measurements are expressed in dB:  
 $P(\text{dB}) = 10 \log(P/P_{\text{ref}})$
- Absolute power measurements are expressed in dBm:  
 $P(\text{dBm}) = 10 \log(P/1 \text{ mW})$

# Types of Power Measurements

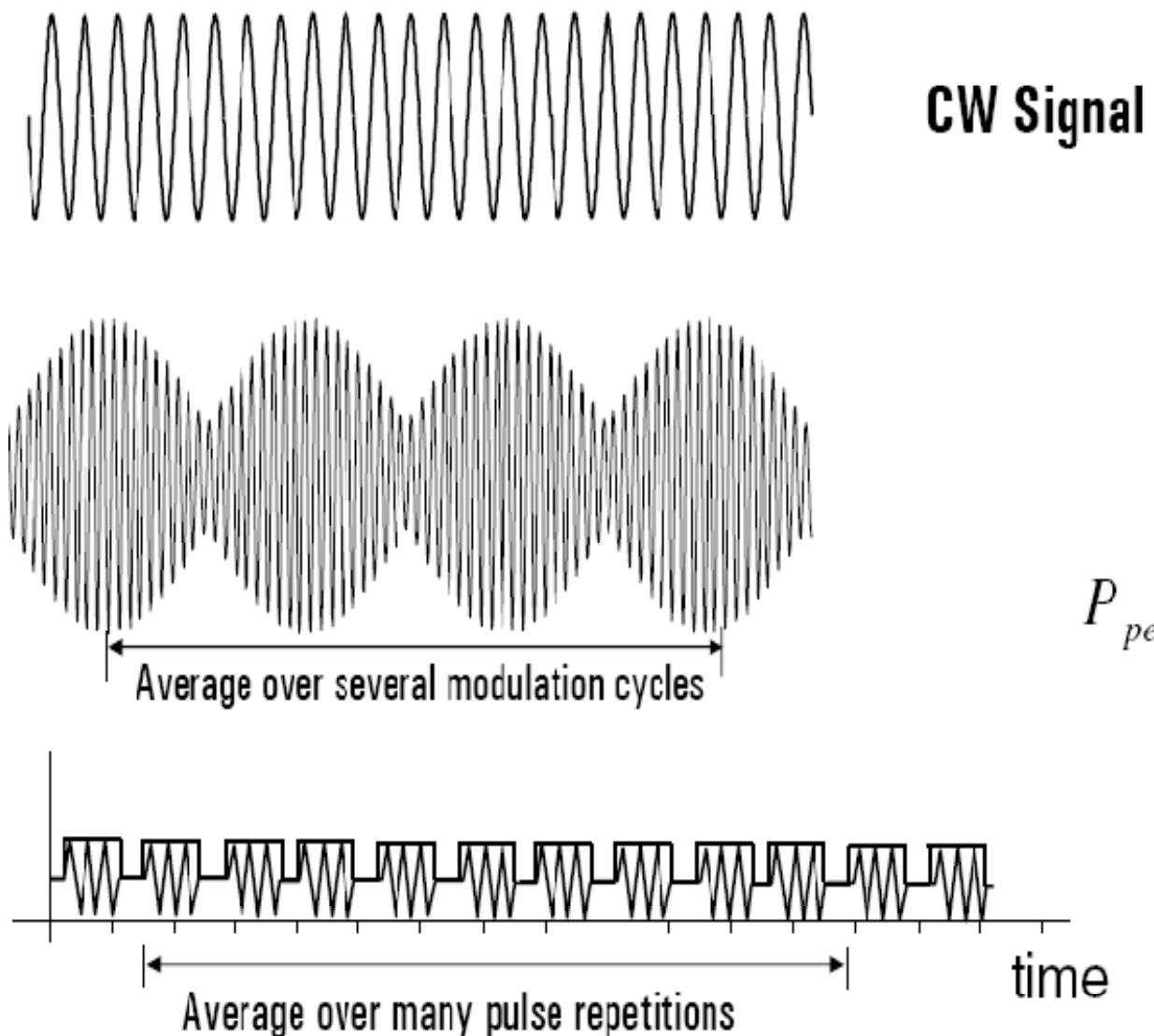


# Instruments to measure microwave power

- Vector Signal Analyzer
- Spectrum Analyzer
- Network Analyzer
- Power Meter and Sensor

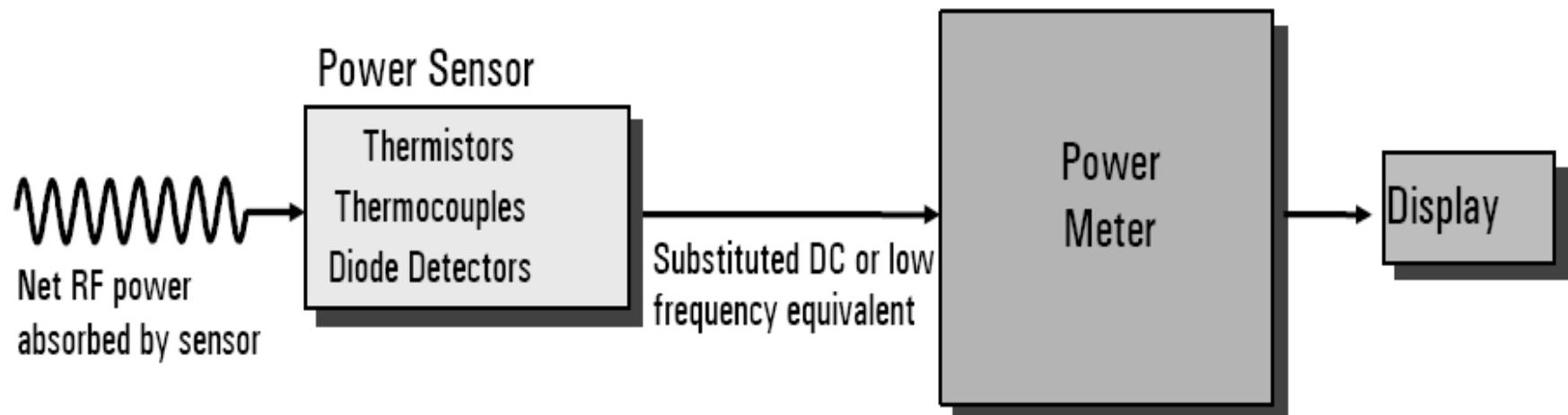


# Average Power

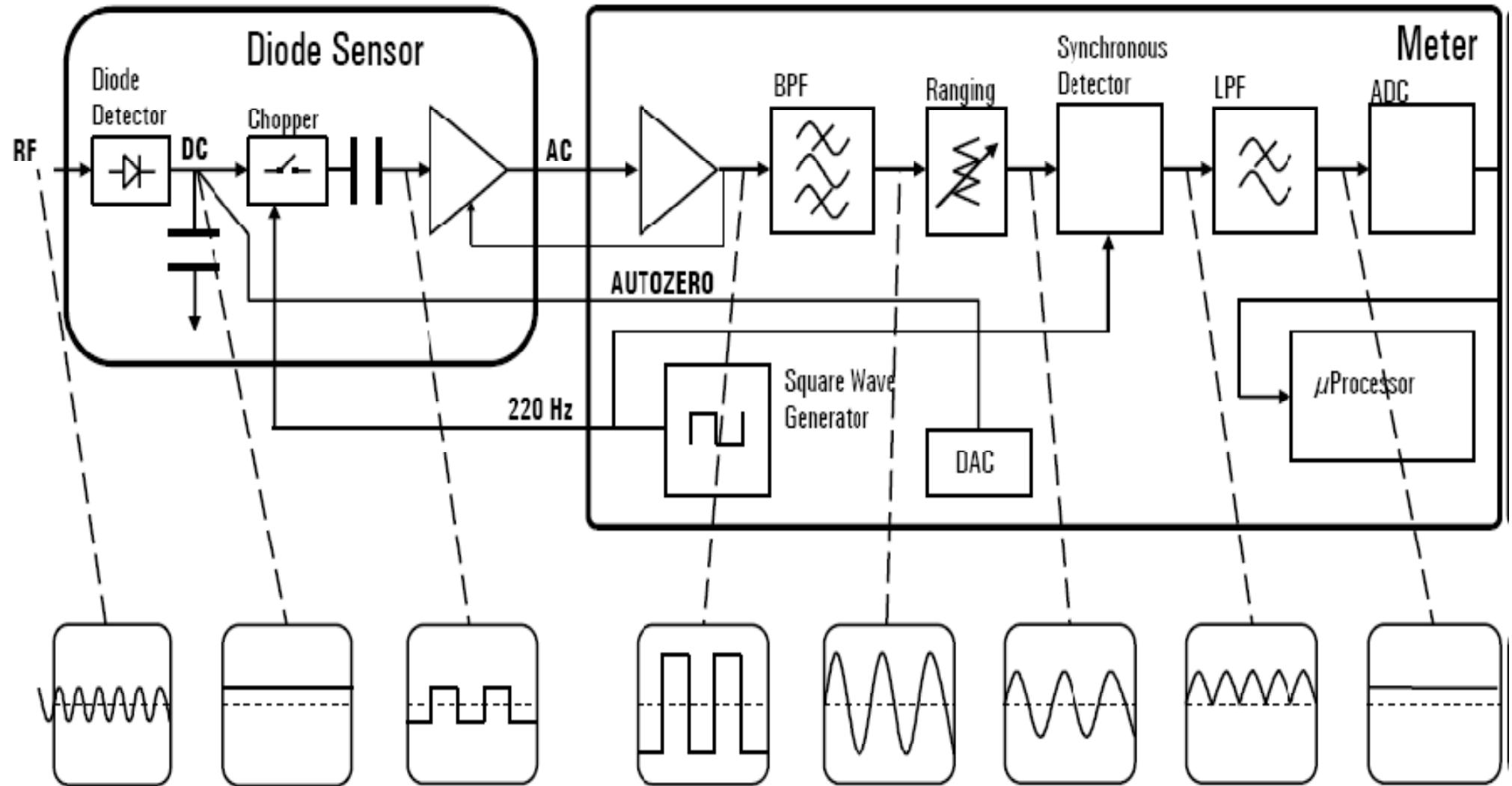


# Basic Measurement Method

## Using a Power Meter



# Basic Measurement Method Explained



# Thermocouples

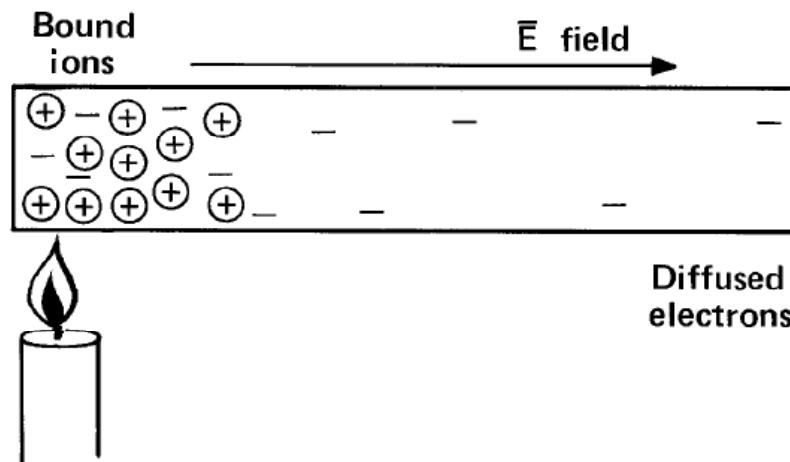


Figure 3-1. Heat at one end of a metal rod gives rise to an electric field.

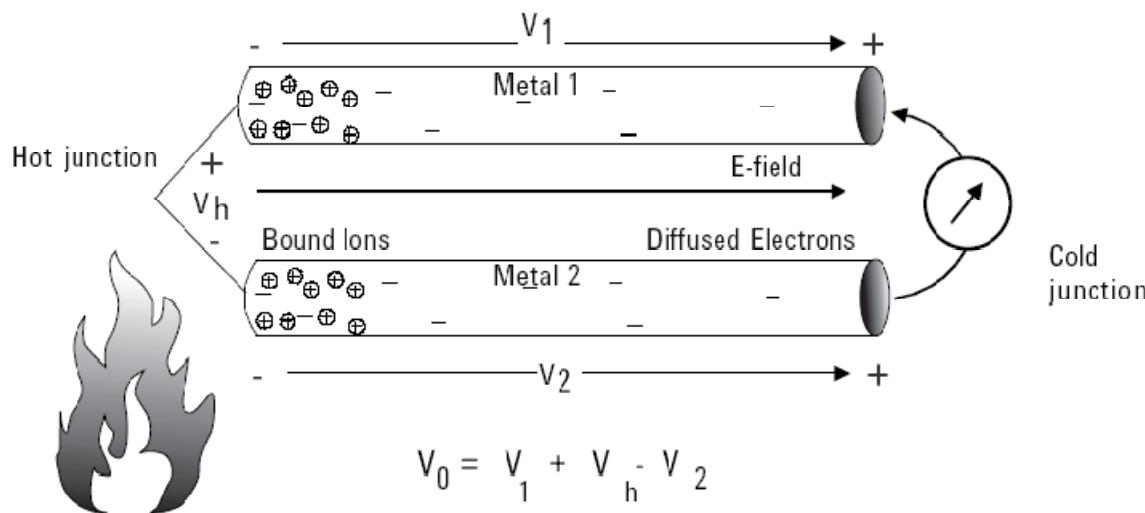


Figure 3-2. Total thermocouple output is the resultant of several thermoelectrical voltages generated along the two-metal circuit.

# Thermocouples

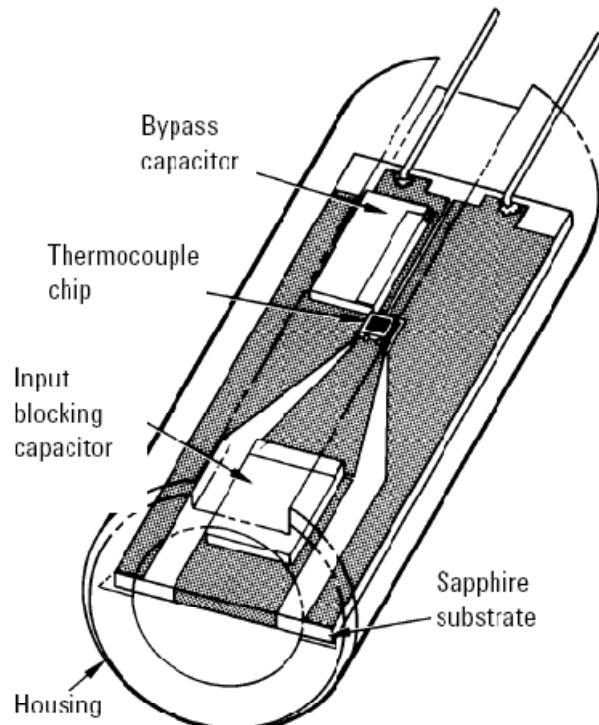


Figure 3-6. Sketch of the thermocouple assembly for the 8481A.

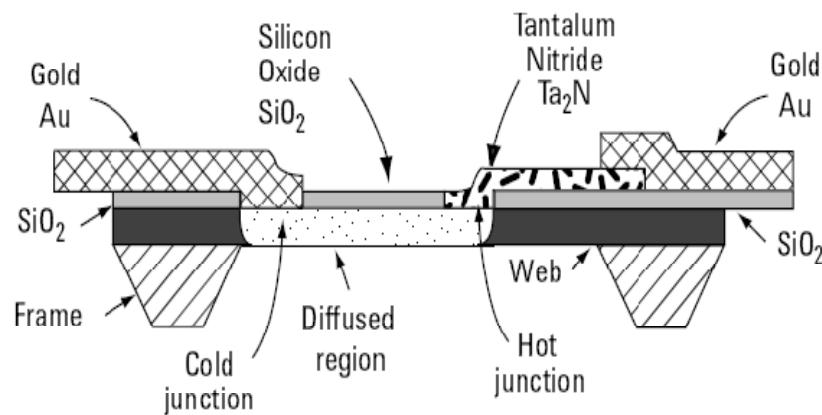


Figure 3-4. Cross section of one thermocouple. Power dissipated in the tantalum-nitride resistor heats the hot junction.

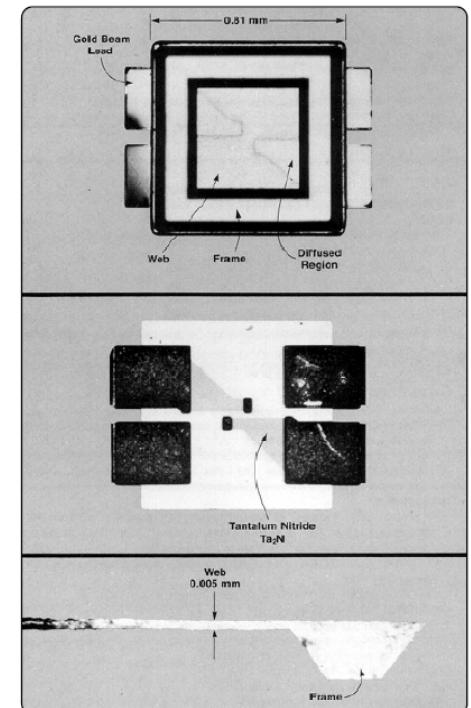
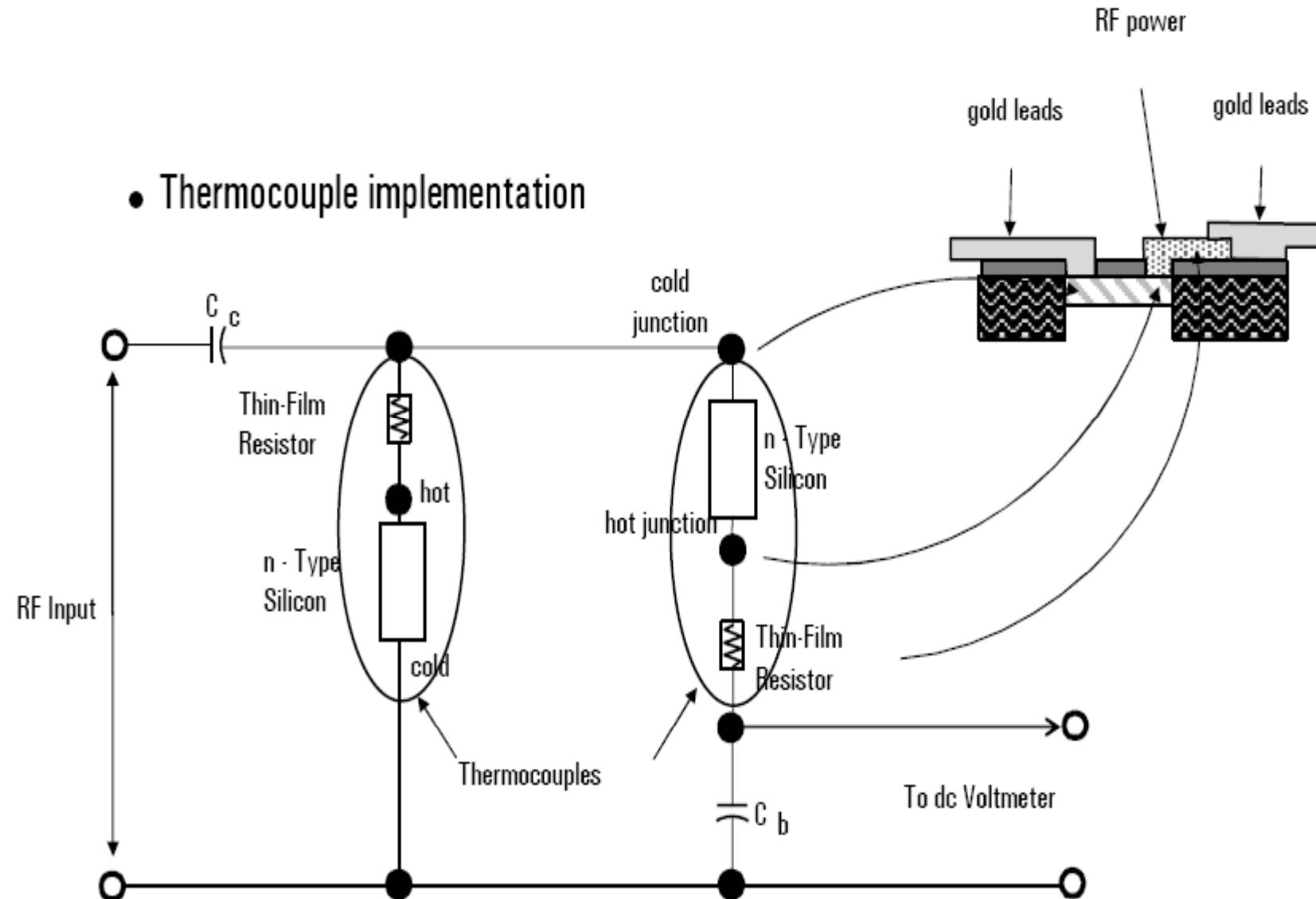


Figure 3-3. Photo-micrograph of the structure of the 8481A thermocouple chip on a thin silicon web.

# Thermocouples



# Thermistors

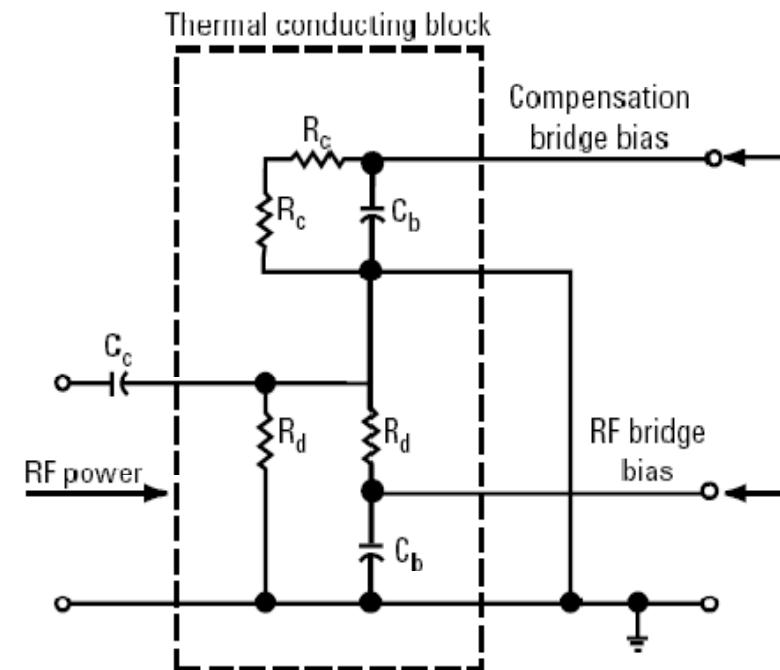
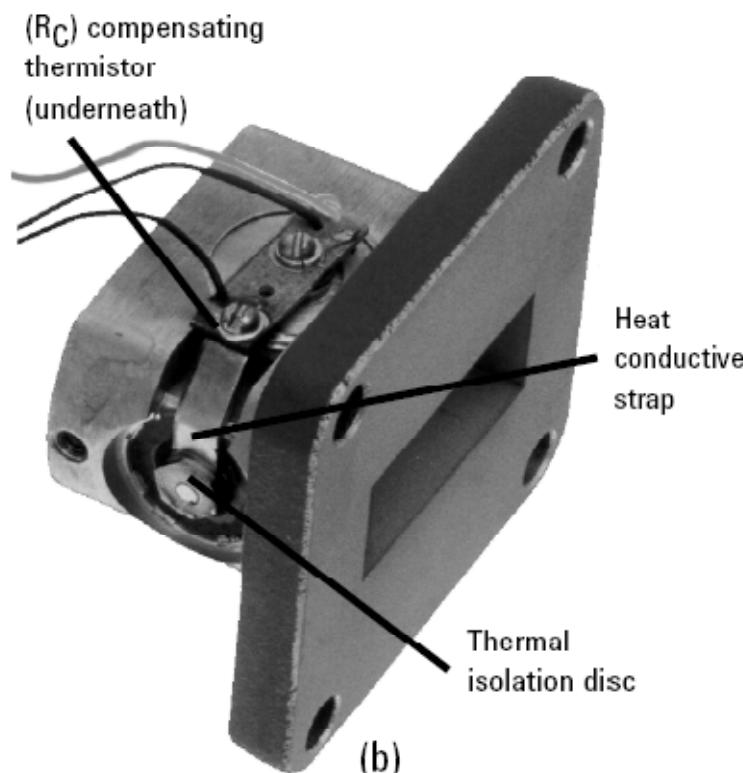
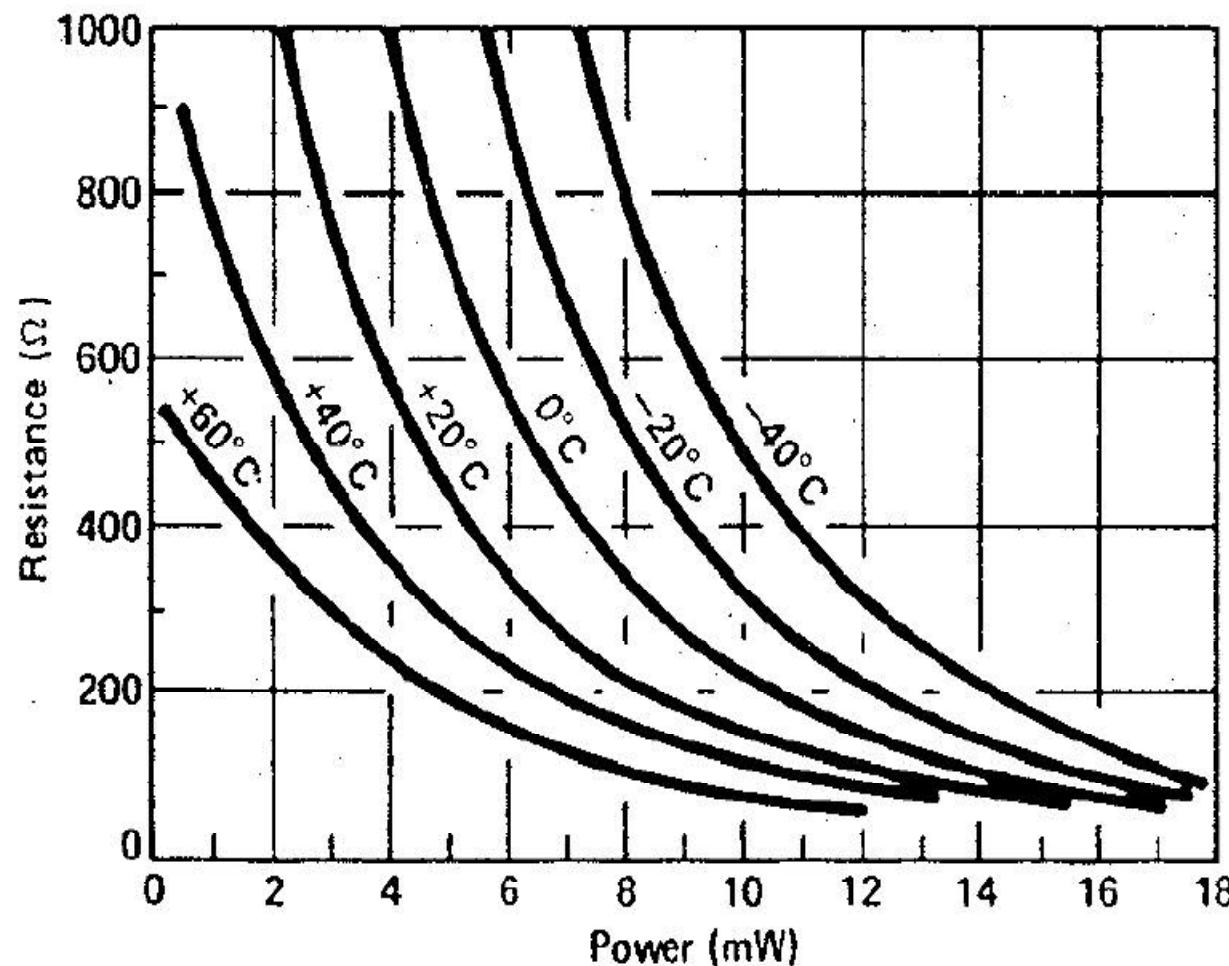


Figure 2-1. 478A coaxial sensor simplified diagram

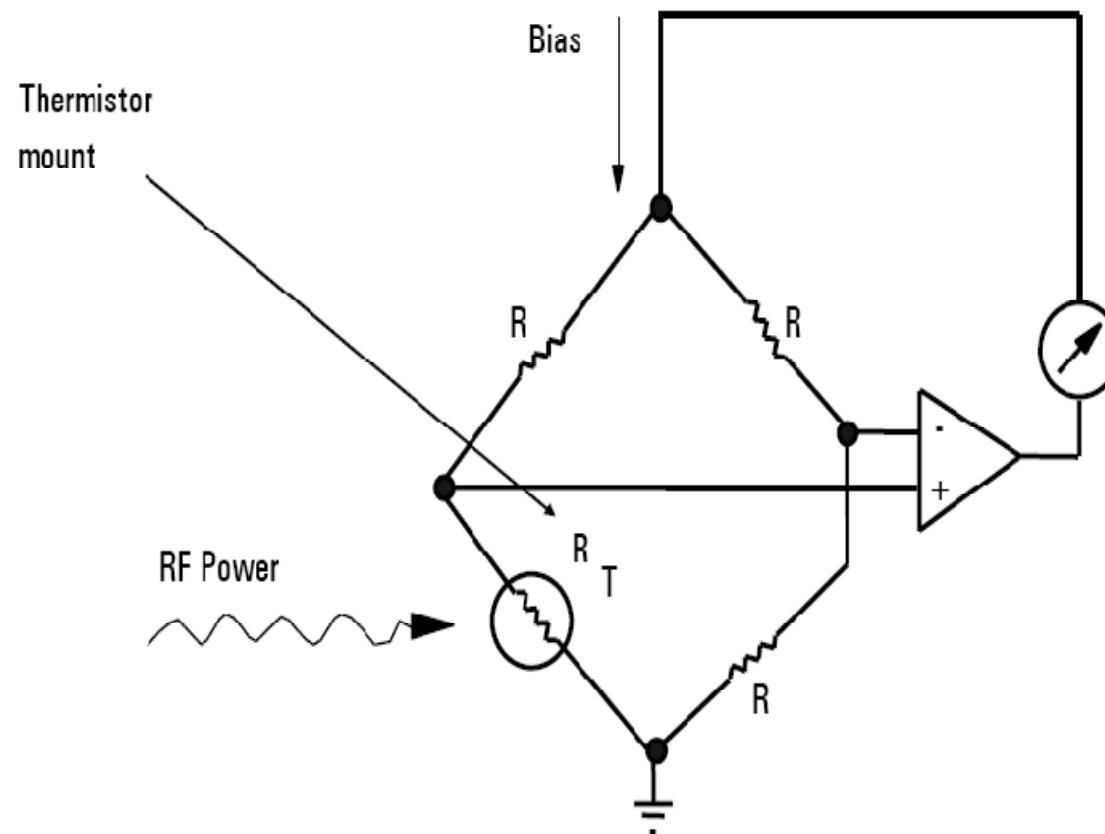
# Thermistors

Characteristic curves of a typical thermistor element



# Thermistors

A self-balancing bridge containing a thermistor



# Thermistors

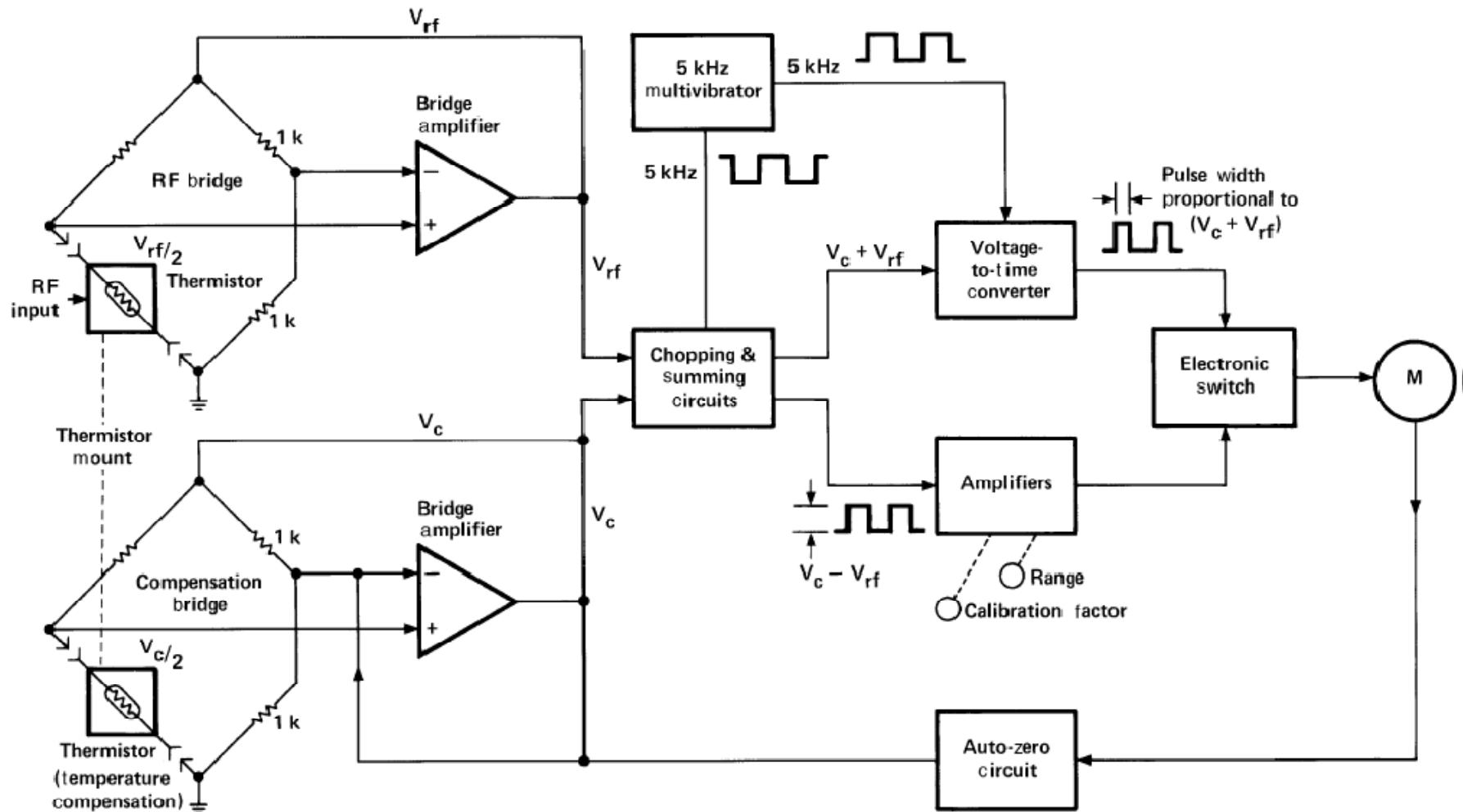
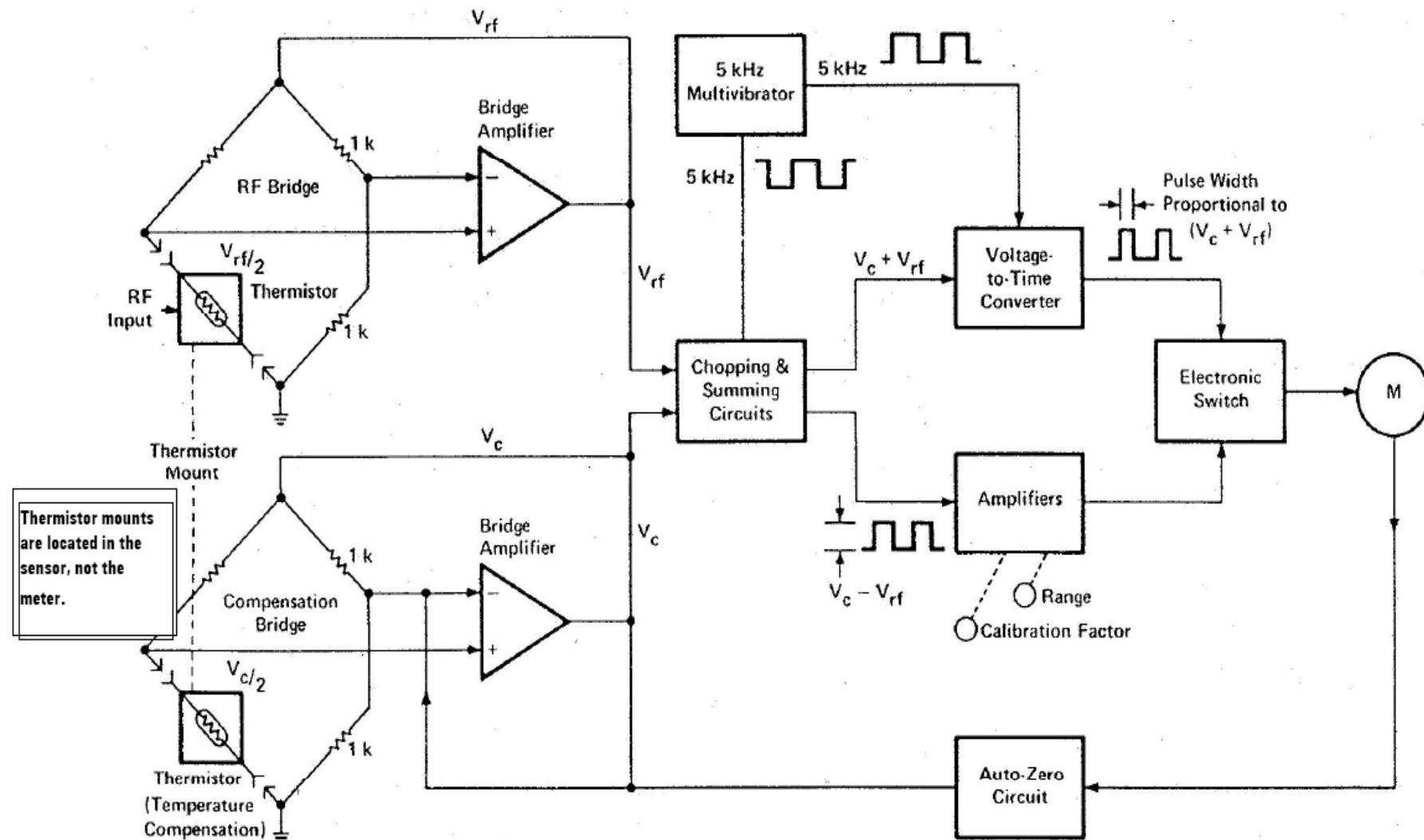


Figure 2-2. Simplified diagram of the 432A power meter.

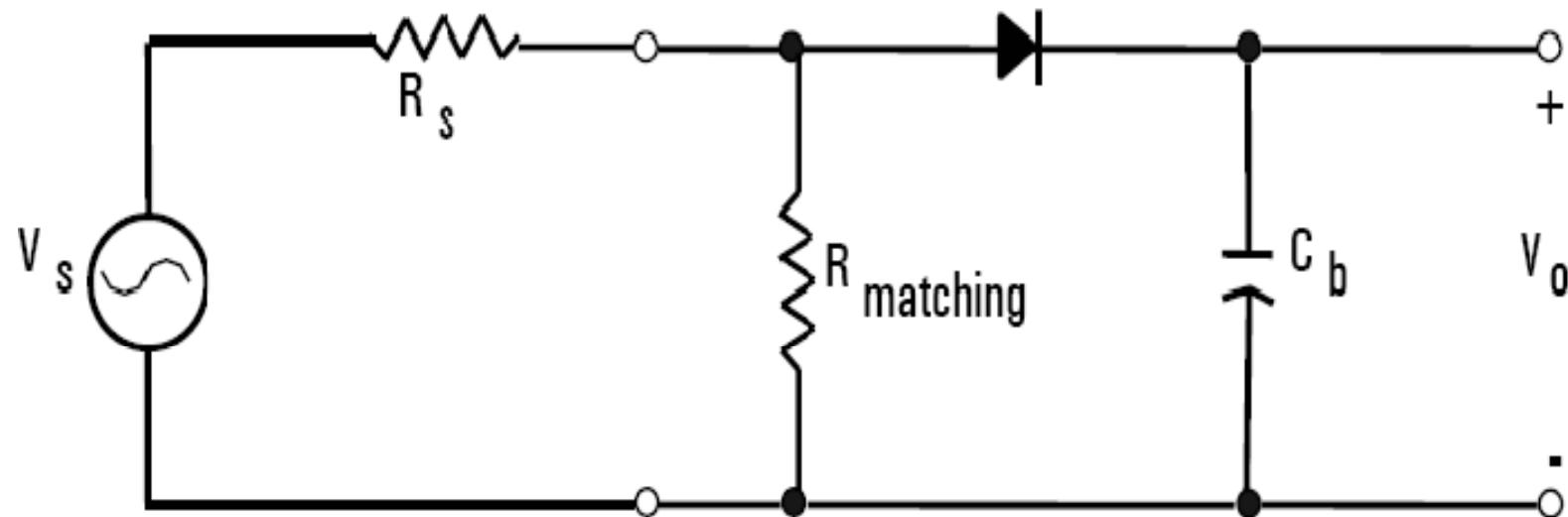
# Power Meters for Thermistor Mounts

- 432A Power Meter

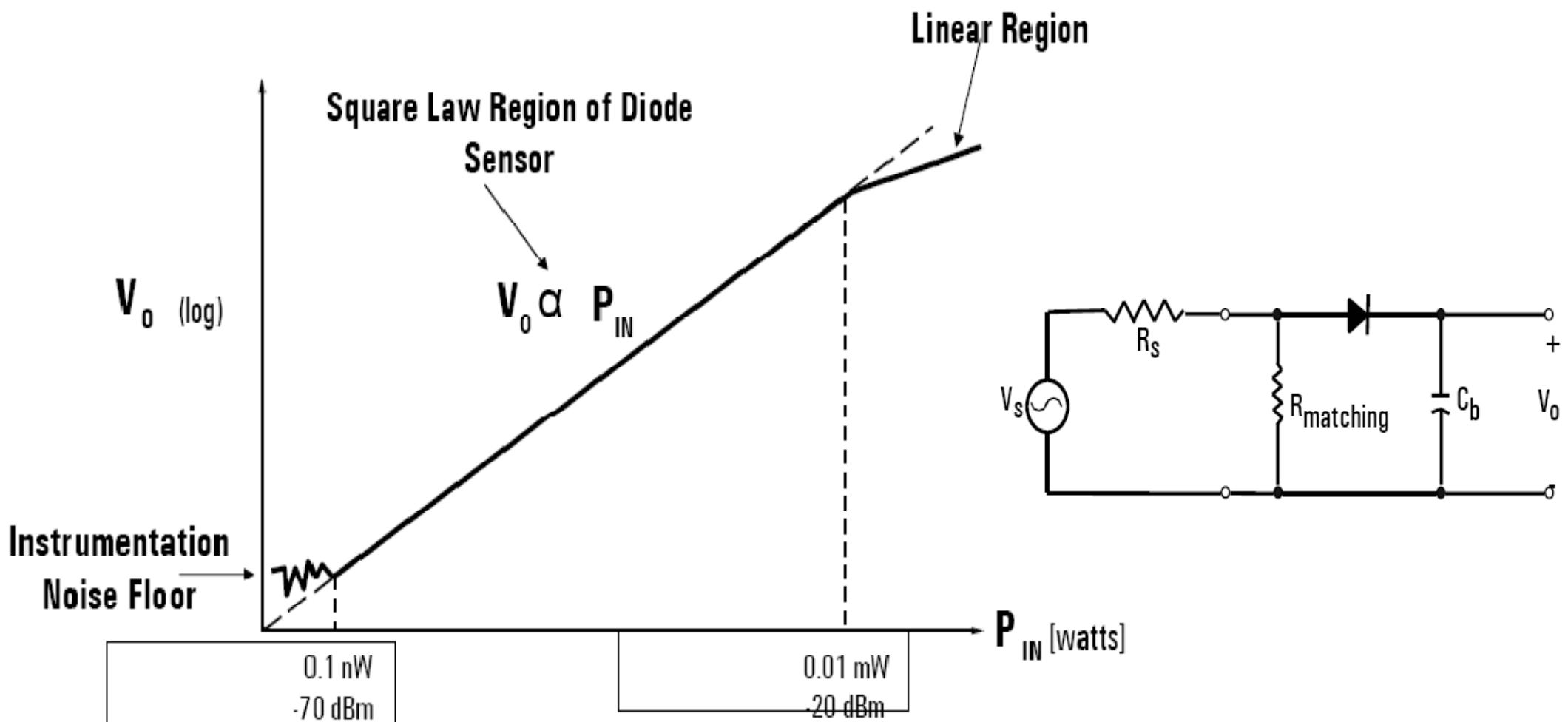


# Diode Detectors

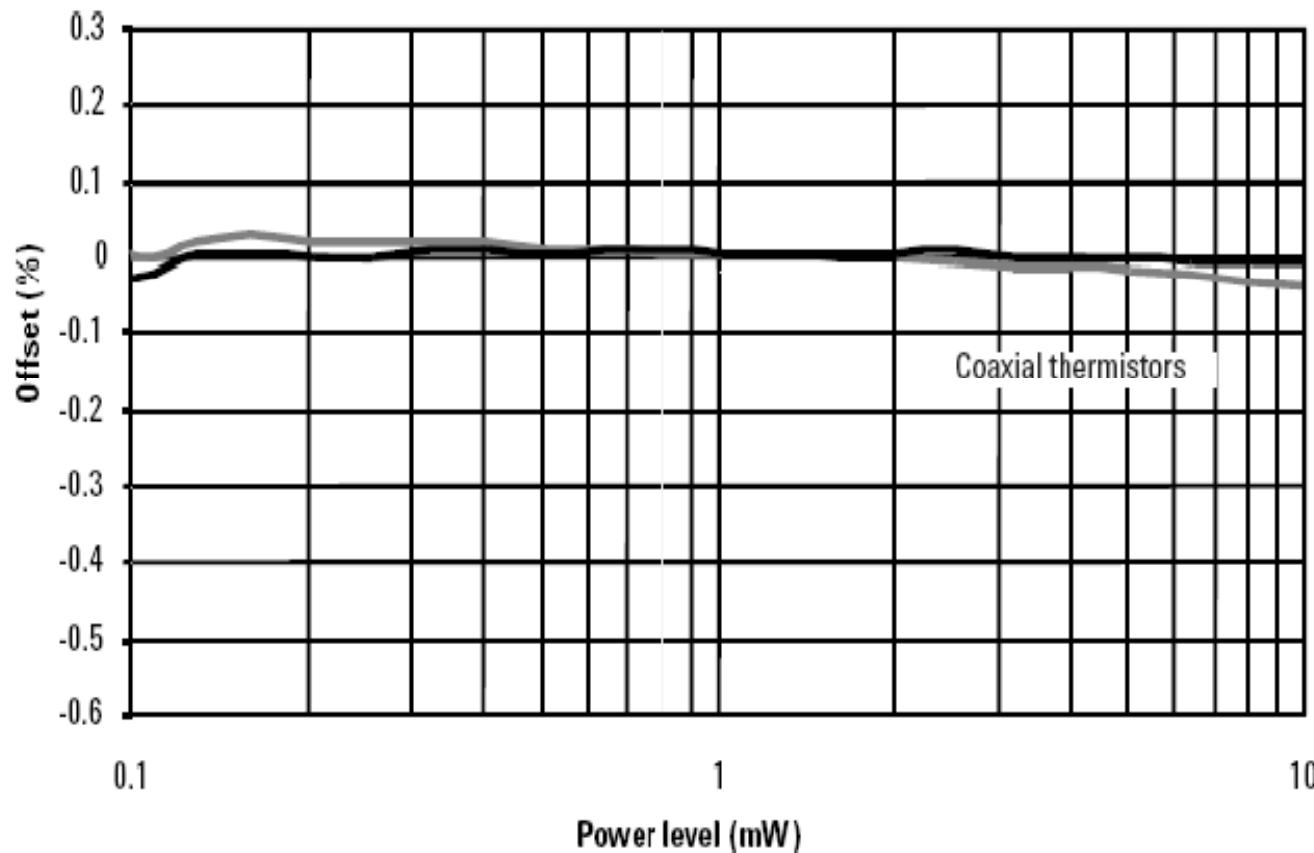
- How does a diode detector work?



# Diode Detectors



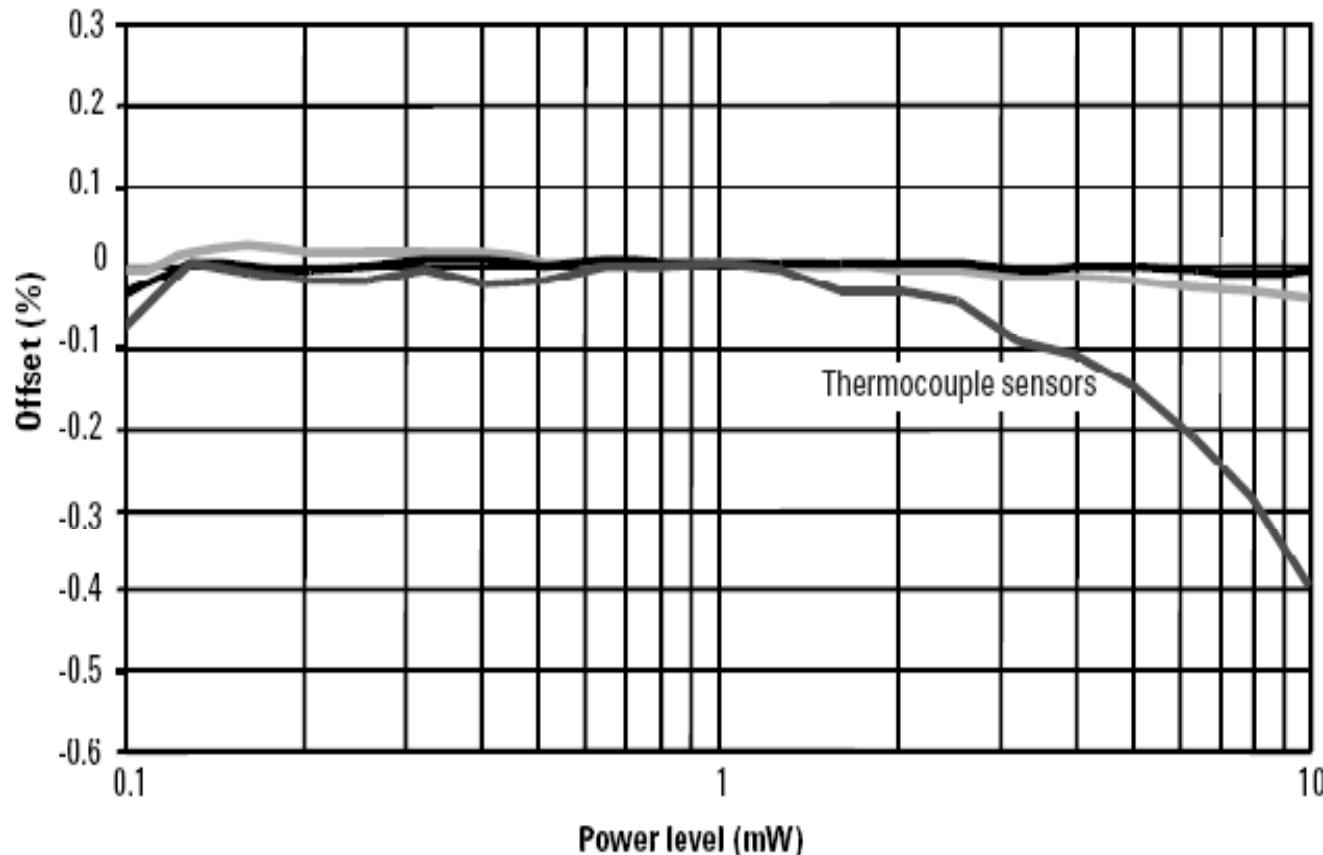
# Sensors linearity



Data courtesy of NPL, Teddington, UK.

**Figure 3-9. Mean linearity of seven units of model 8478A coaxial thermistor sensors from 0.1 to 10 mW. (8478A is an older model, the current model is 8478B.)**

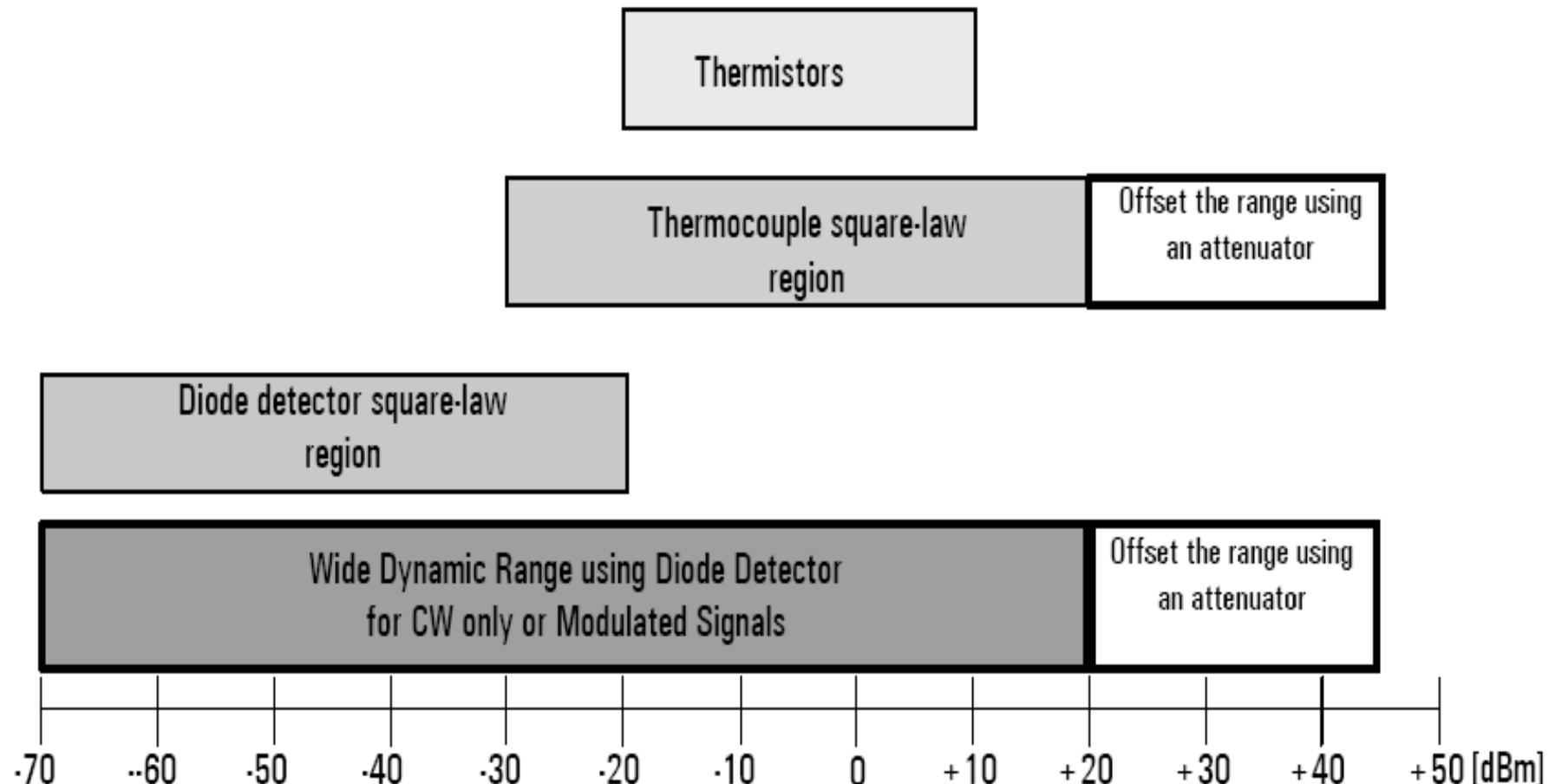
# Sensors linearity



Data courtesy of NPL, Teddington, UK.

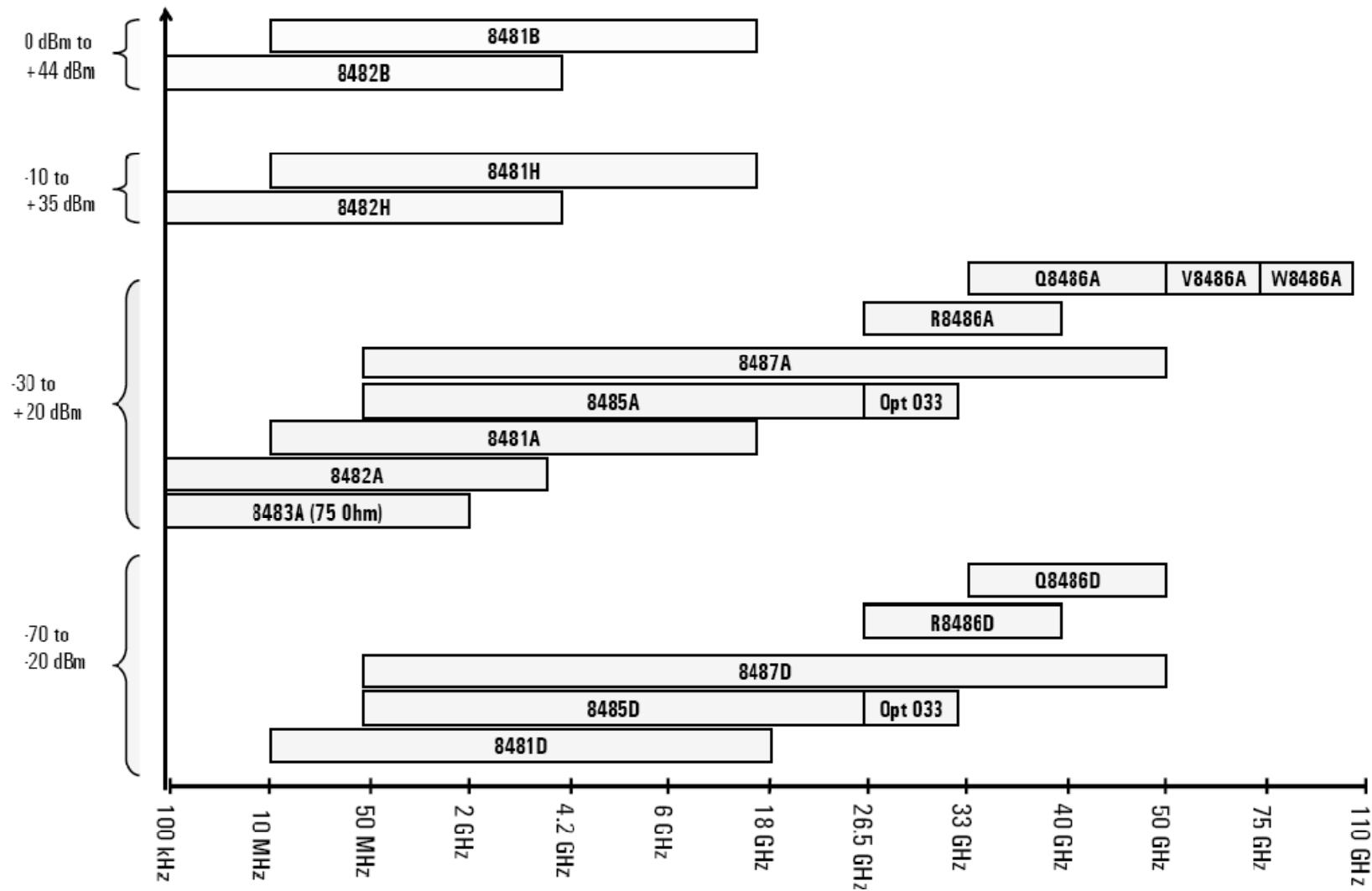
**Figure 3-10. Mean linearity of four units of model 8481A coaxial thermocouple sensors from 0.1 to 10 mW.**

# Power Ranges of the Various Sensors

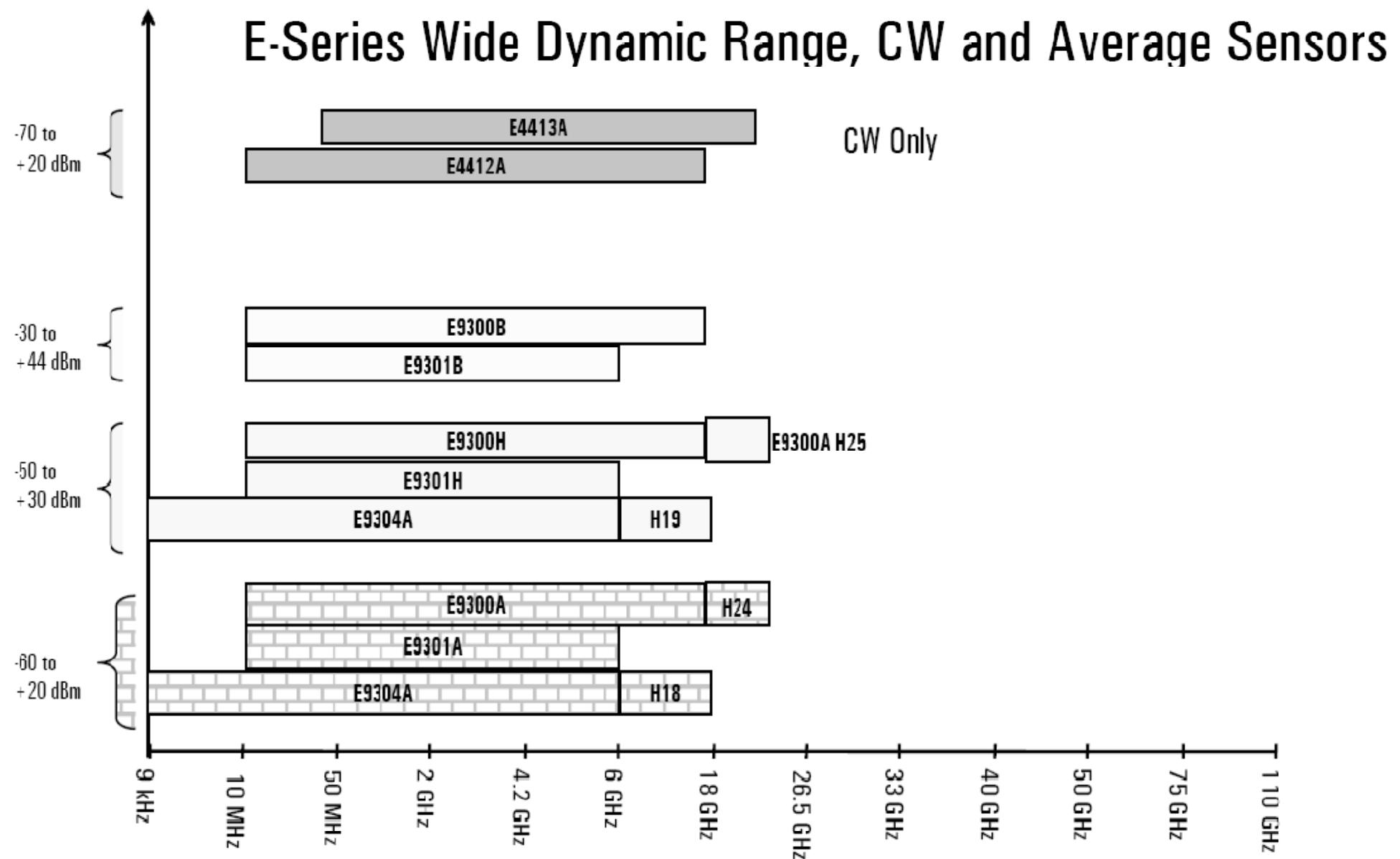


# Agilent Power Sensor Selection Guide

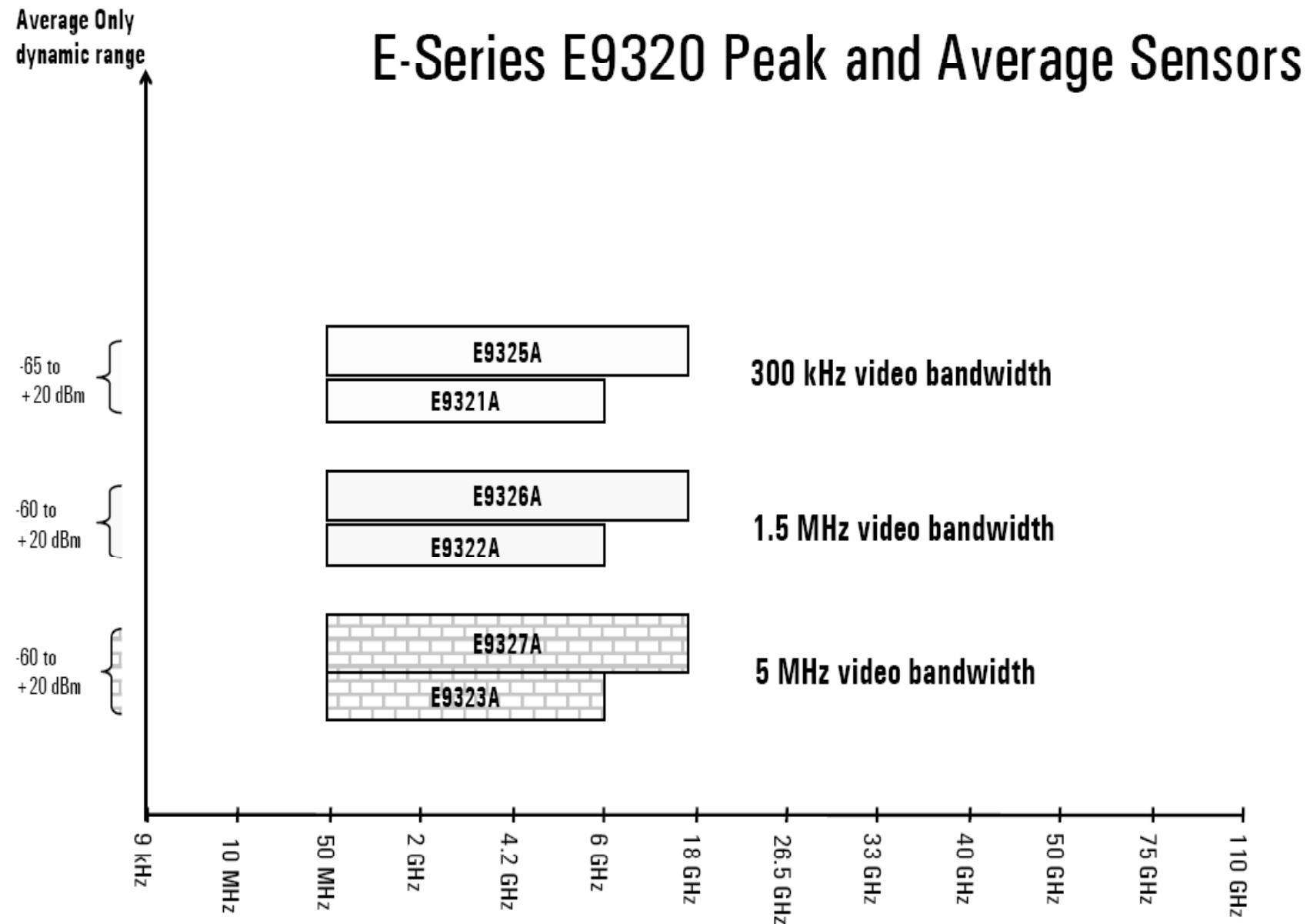
## 8480 Series



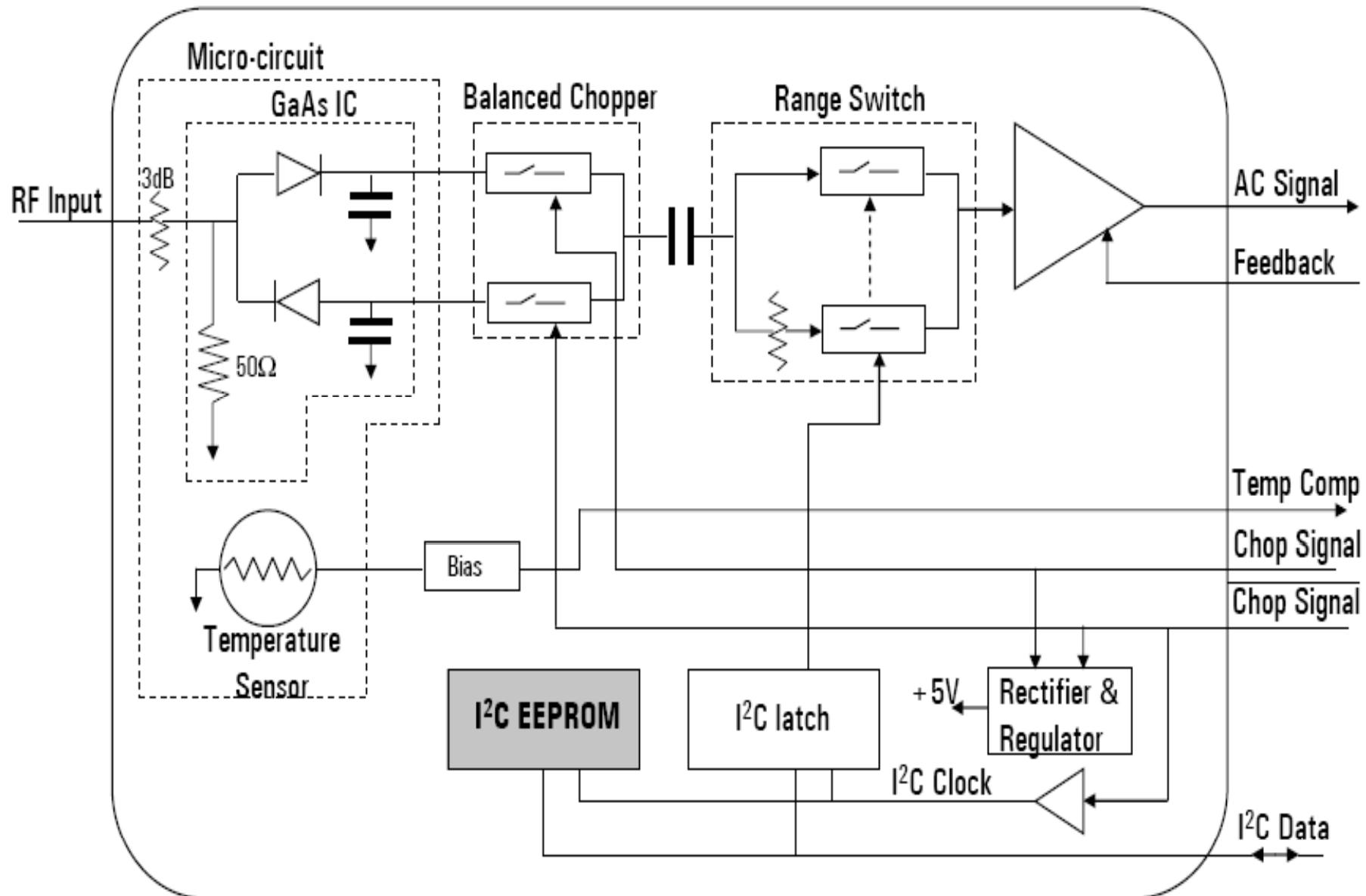
# Agilent Power Sensor Selection Guide



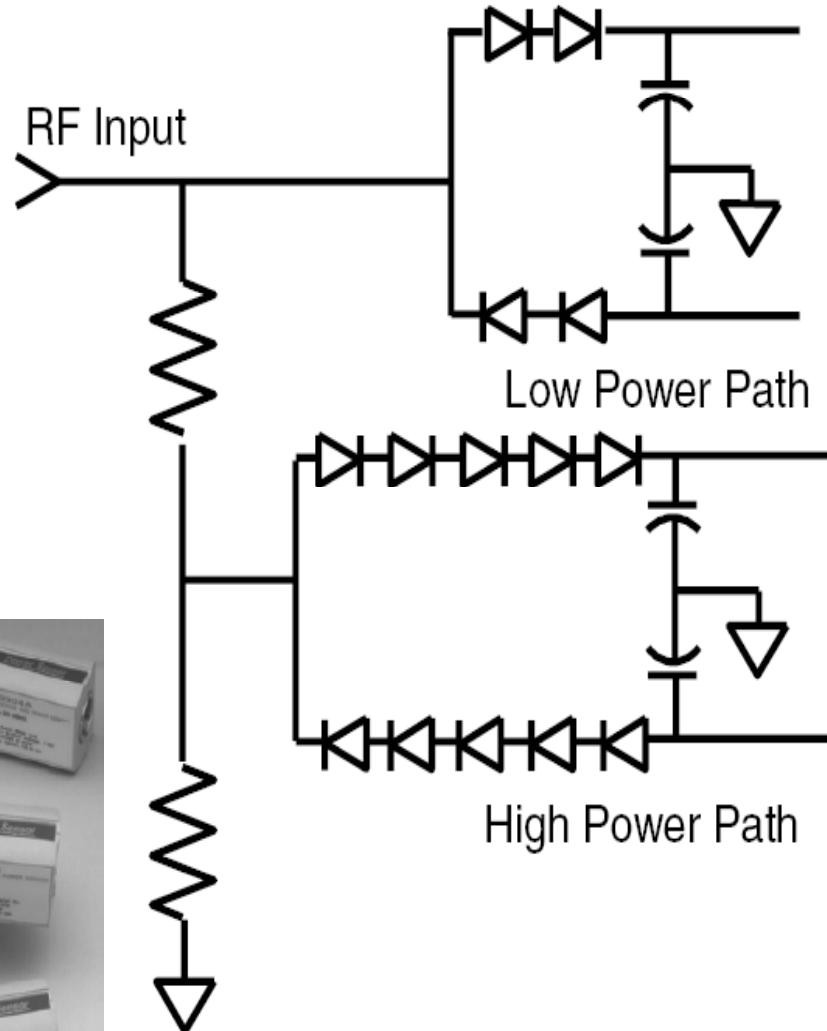
# Agilent Power Sensor Selection Guide



# Wide-Dynamic-Range CW-only Sensors



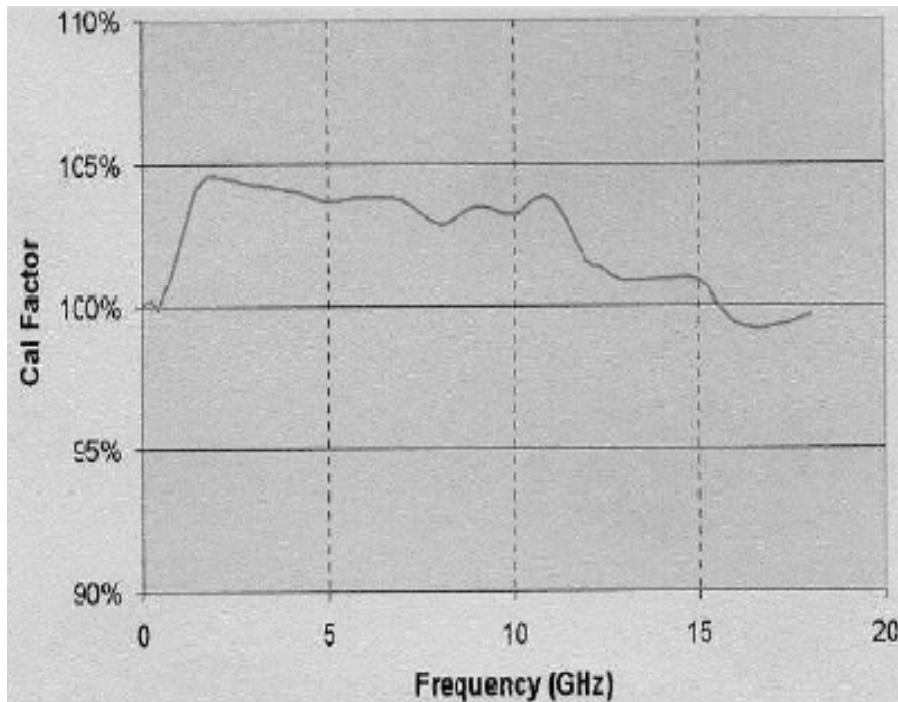
# Agilent E9300 Average Power Sensors



Innovative Design:

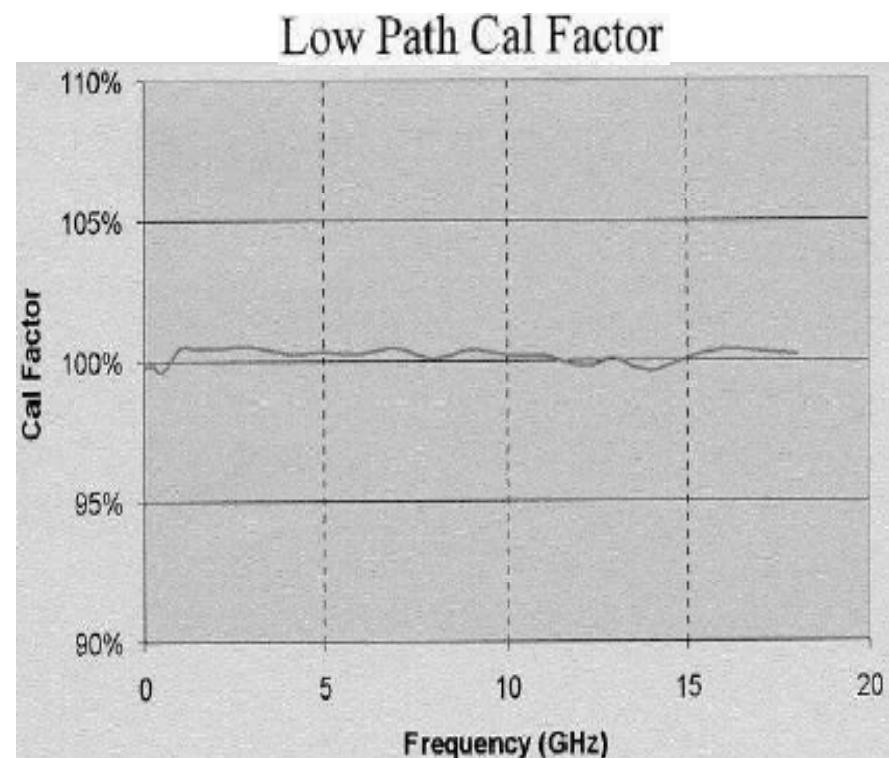
- Diode stack- attenuator-diode stack topology
- Two paths with an automatic switch point

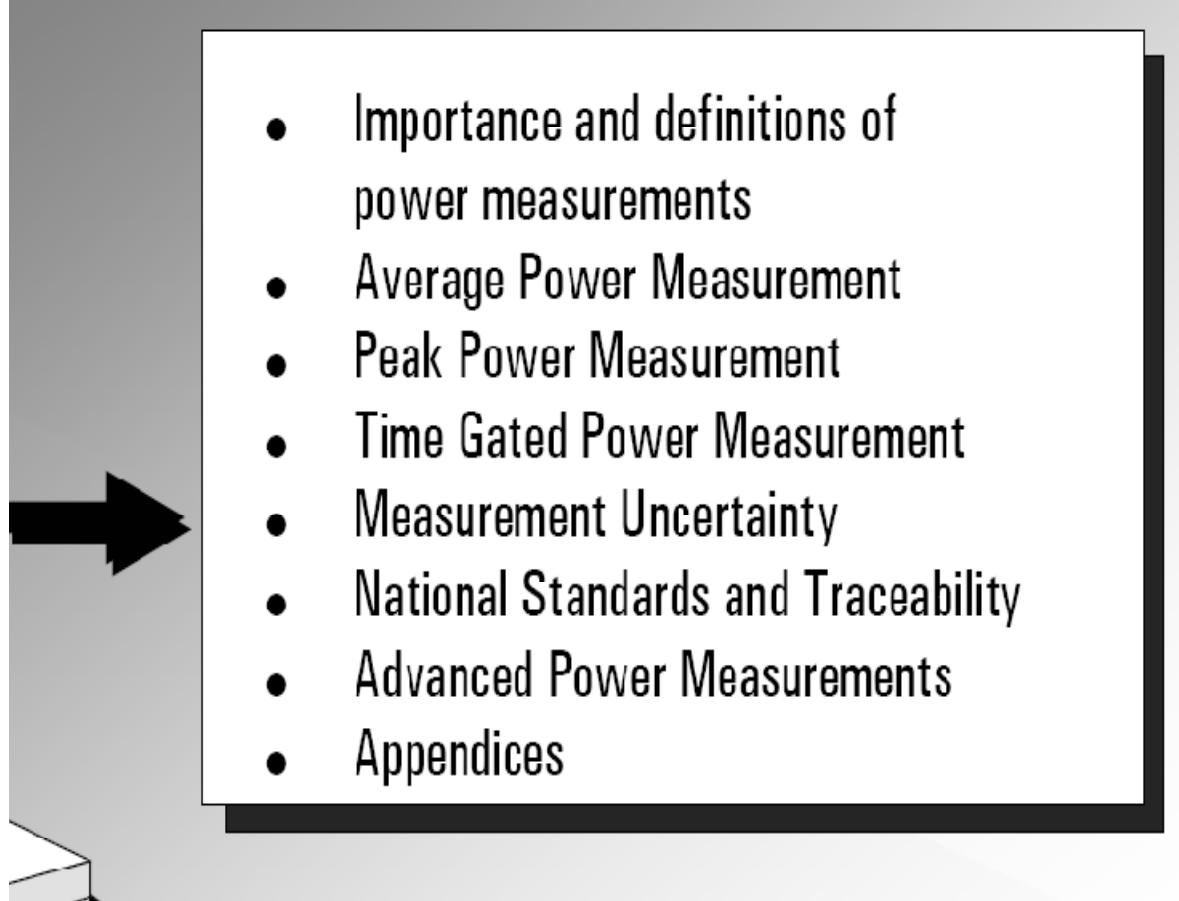
# Agilent E9300 Average Power Sensors



High Path Cal Factor

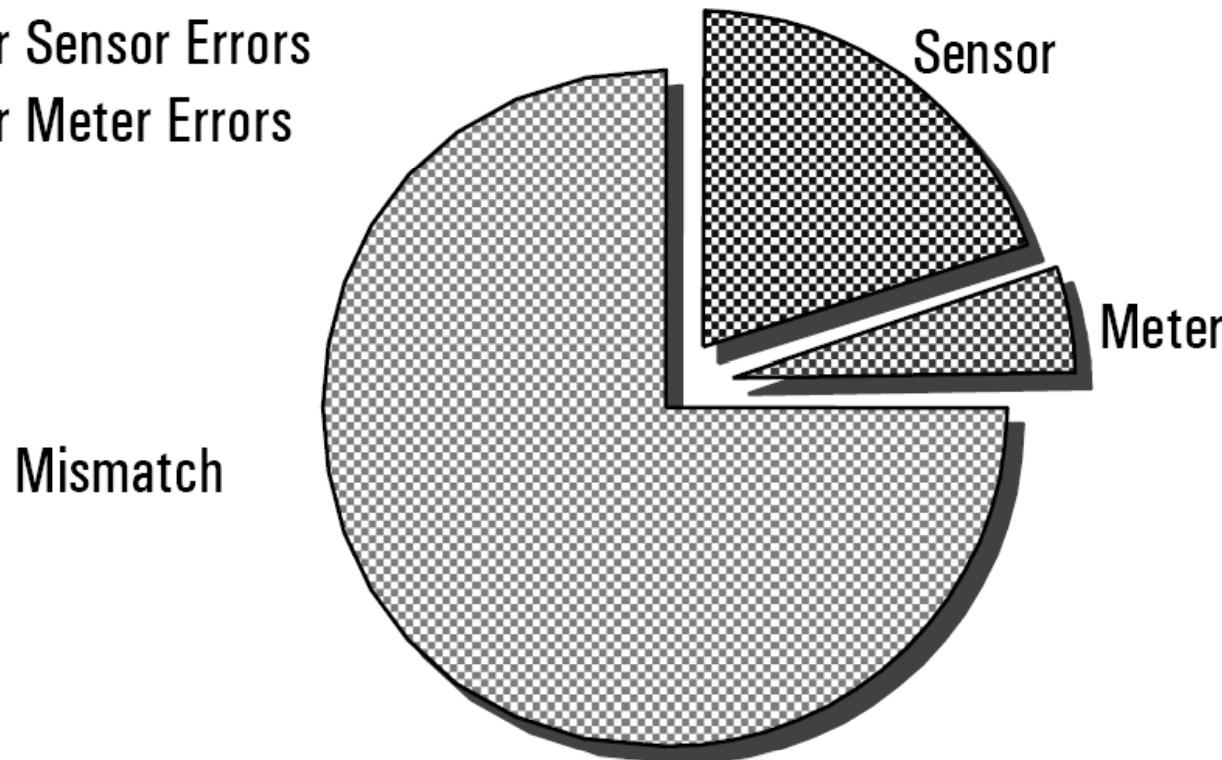
Flat calibration factors give accurate measurement of multi-tone signals.



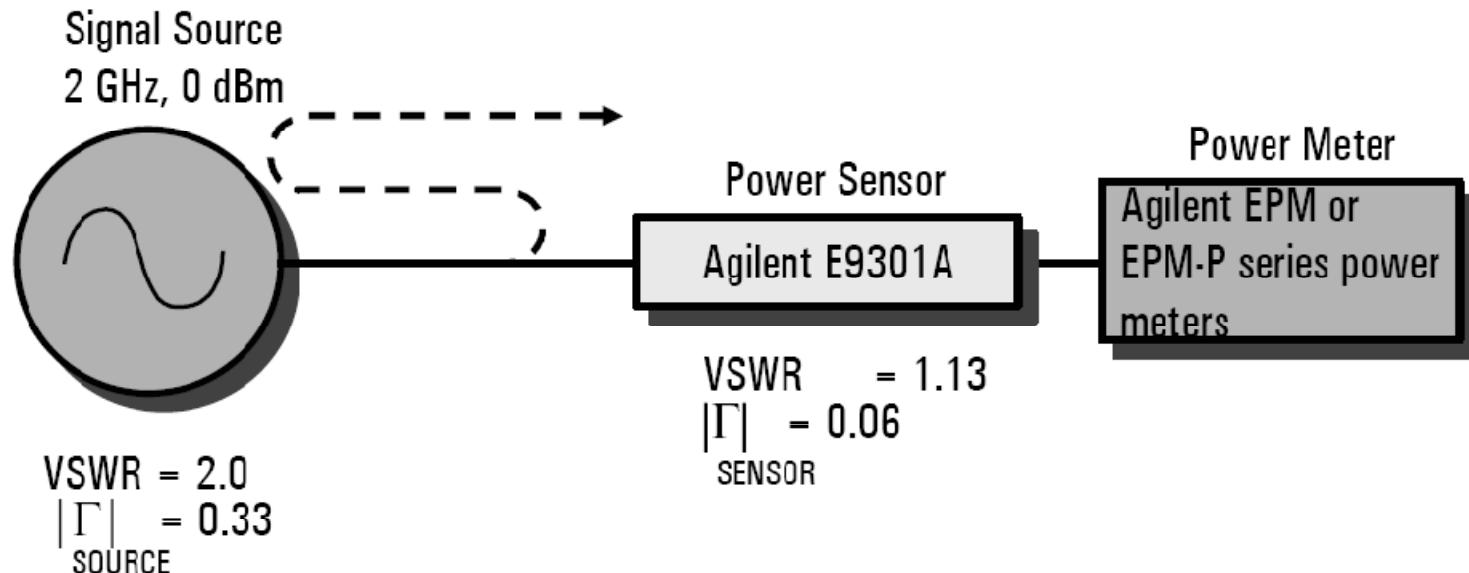


# Power measurement uncertainty sources

- Sensor and Source Mismatch Errors
- Power Sensor Errors
- Power Meter Errors



# Calculation of Mismatch Uncertainty

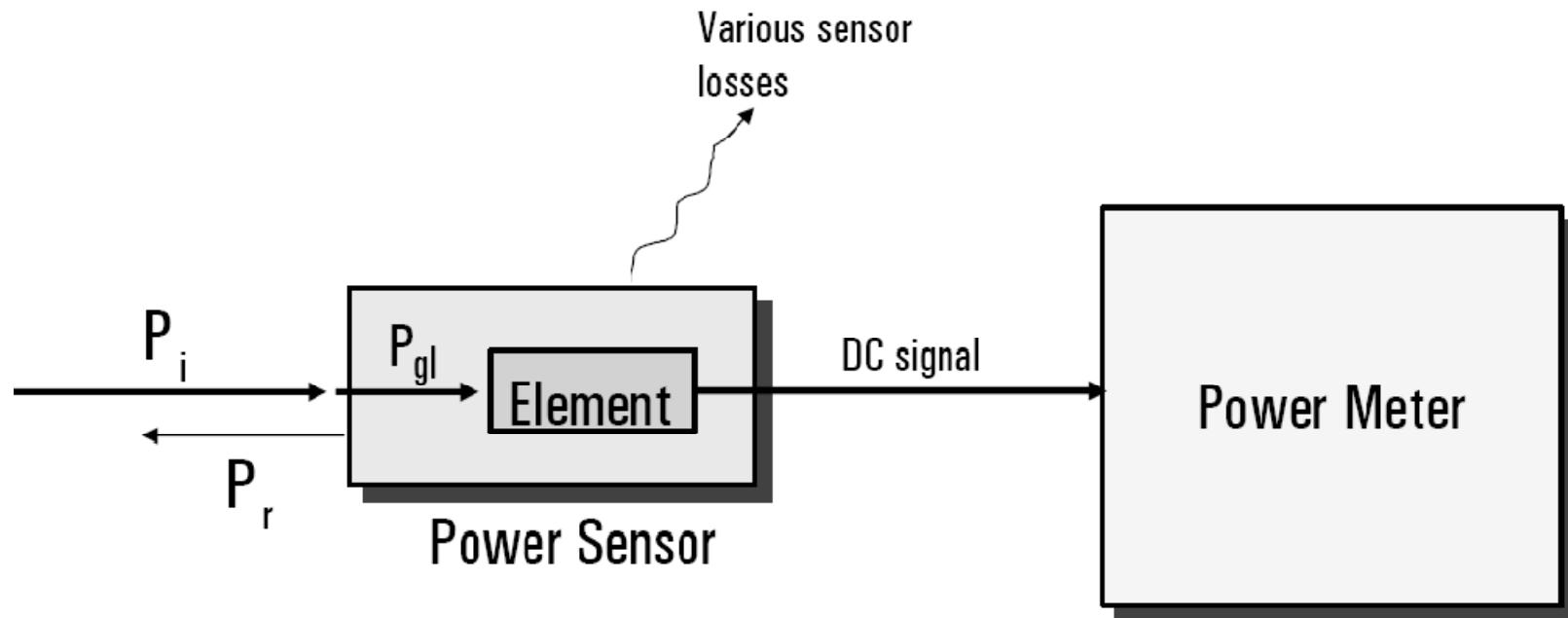


$$\text{Mismatch Uncertainty} = \pm 2 \times |\Gamma|_{\text{SOURCE}} \times |\Gamma|_{\text{SENSOR}} \times 100\%$$

$$\text{Mismatch Uncertainty} = \pm 2 \times 0.33 \times 0.06 \times 100\% = \pm 3.96\%$$

$$|\Gamma| = \frac{\text{VSWR} \cdot 1}{\text{VSWR} + 1}$$

# Power Sensor Uncertainties



Cal Factor:  $K_b = \eta_e \frac{P_{gl}}{P_i}$

$P_i$  = incident power;  $P_r$  = reflected power

$P_{gl}$  = net power transferred to the load from the generator

$\eta_e$  = Effective Efficiency

# Power Meter Instrumentation Uncertainties

Noise



Power reference uncertainty

Drift

Zero Set

Instrumentation uncertainty

# What is an acceptable meas. uncertainty?



- Reasonable Error Limits:
  - 0.5 dB?
  - or 12%

Which is the larger error?

# Calculating Power Meas. Uncertainty

Mismatch uncertainty:  $\pm 3.96\%$

Power Linearity:  $\pm 2.0\%^1$

Cal Factor uncertainty:  $\pm 1.8\%^1$

Power reference uncertainty:  $\pm 1.07\%^1$

Instrumentation uncertainty:  $\pm 0.5\%$

<sup>1</sup> Specifications apply for an E9301A sensor and EPM or EPM-P series power meter, over  $25 \pm 10$  degrees C temperature range

*Now that the uncertainties have been determined, how are they combined?*

# Worst-Case Uncertainty

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- In our example worst case uncertainty would be:

$$= 3.96\% + 2.0\% + 1.8\% + 1.07\% + 0.5\% = \pm 9.33\%$$

$$+ 9.33\% = 10 \log (1 + 0.093) = +0.39 \text{ dB}$$

$$- 9.33\% = 10 \log (1 - 0.093) = -0.42 \text{ dB}$$

# Combining the Measurement Uncertainties

Source of Uncertainty	Value $\pm \%$	Probability Distribution	Divisor	Standard Uncertainty $u_i (k=1)$
Source/Sensor Mismatch at 2 GHz	3.96	U-shaped	1.414	2.8
Calibration Factor Uncertainty at 2 GHz	2.0	Normal	2	1.0
Linearity at 0 dBm	1.8	Normal	2	0.9
Power Reference Uncertainty	1.07	Normal	2	0.53
Instrumentation Uncertainty	0.5	Normal	2	0.25

Combined Standard Uncertainty  $u_c = \text{RSS of } u_i$

Expanded Uncertainty ( $k=2$ ) =  $2 \times u_i$

# Combined Standard Uncertainty

---

- In our example, the  $u_c$  would be:

$$= \sqrt{(2.8)^2 + (1.0)^2 + (0.9)^2 + (0.53)^2 + (0.25)^2}$$

$$= \pm 3.16\%$$

- The Expanded Uncertainty ( $u$ ) =  $2 \times 3.16 = \pm 6.32\%$

$$+ 6.3\% = 10 \log (1 + 0.063) = +0.27 \text{ dB } (+0.39 \text{ dB worst case})$$

$$- 6.3\% = 10 \log (1 - 0.063) = -0.28 \text{ dB } (-0.42 \text{ dB worst case})$$

# National Standards and Traceability

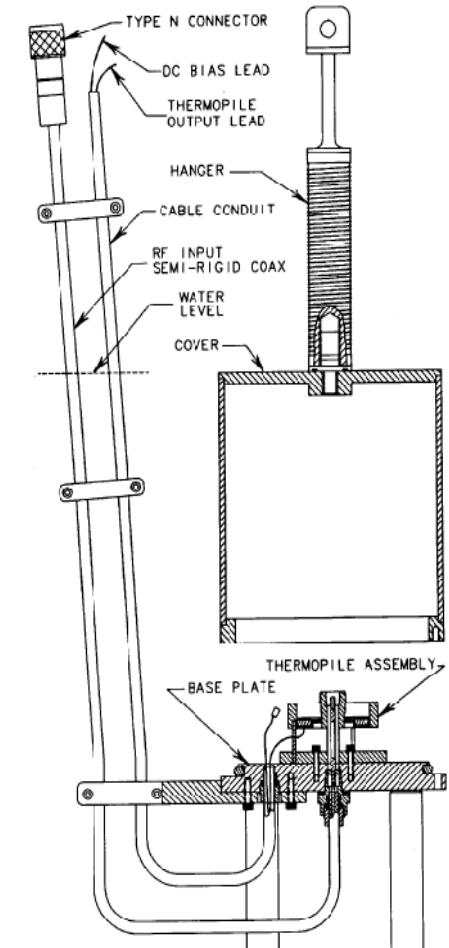
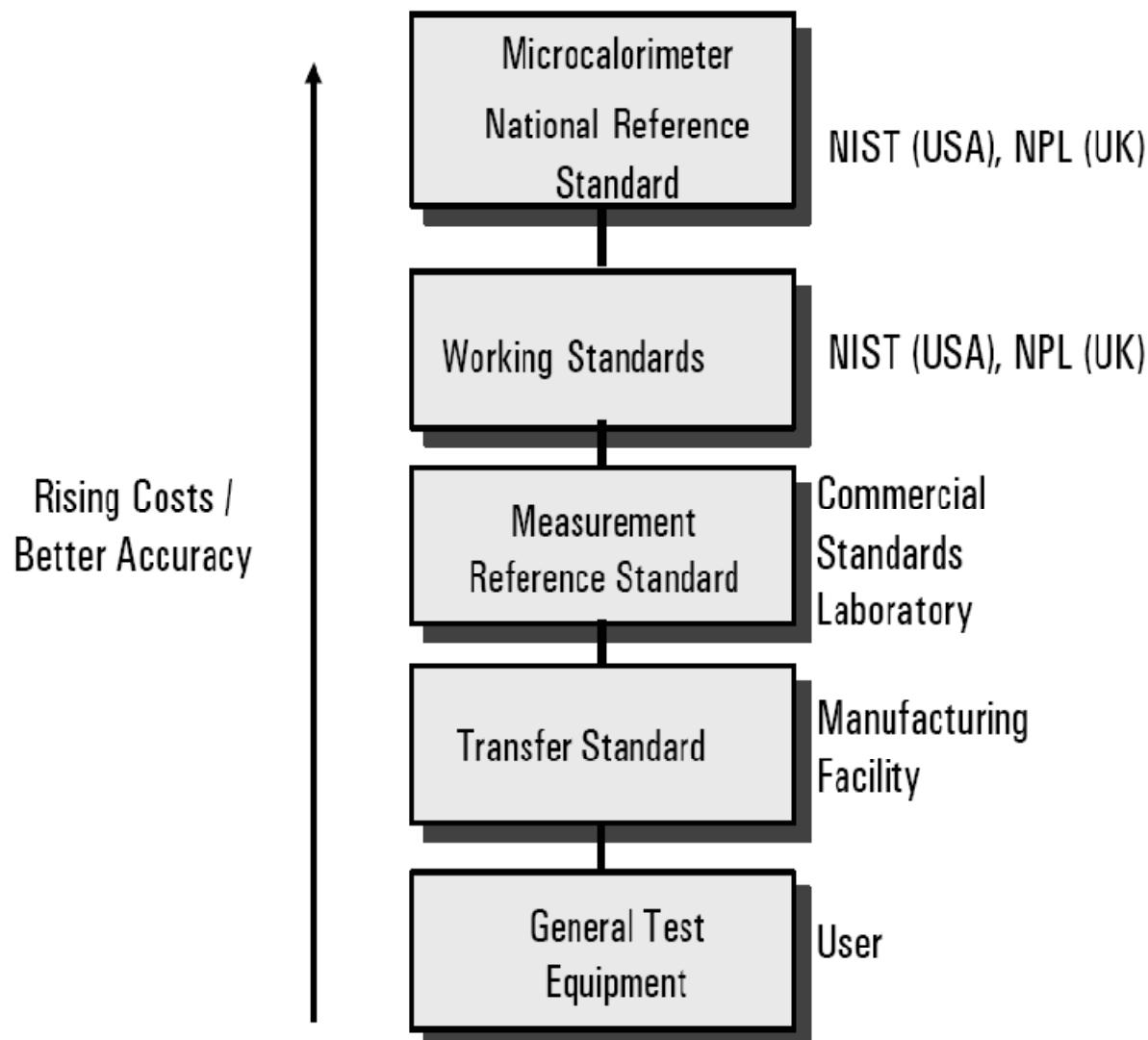


Figure 3-2. Schematic cross-section of the NIST coaxial microcalorimeter at Boulder, CO. The entire sensor configuration is maintained under a water bath with a highly-stable temperature so that RF to DC substitutions may be made precisely.